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Wilder et al.

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(45) **Date of Patent: Apr. 15, 2014**

(54) **AERONAUTICAL HOLDING PATTERN CALCULATION FOR SOLVING HIGH WIND AND PROTECTED AIRSPACE ISSUES**

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(73) Assignee: **Epoch Flight Systems LLC**, Frisco, TX (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(22) Filed: **Mar. 11, 2013**

(51) **Int. Cl.**
B64D 1/00 (2006.01)

(52) **U.S. Cl.**
USPC **701/423**; 701/3; 701/120; 701/122; 701/425; 701/487; 701/10

(58) **Field of Classification Search**
None
See application file for complete search history.

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U.S. Department of Transportation Federal Aviation Administration, FAA-H-8083-15B: Instrument Flying Handbook, 2012, pp. 1-4, 301-304, and 346-365.*
U.S. Department of Transportation Federal Aviation Administration Order 7130.3A: Holding Pattern Criteria, Mar. 18, 1998, pp. 1-61.*

* cited by examiner

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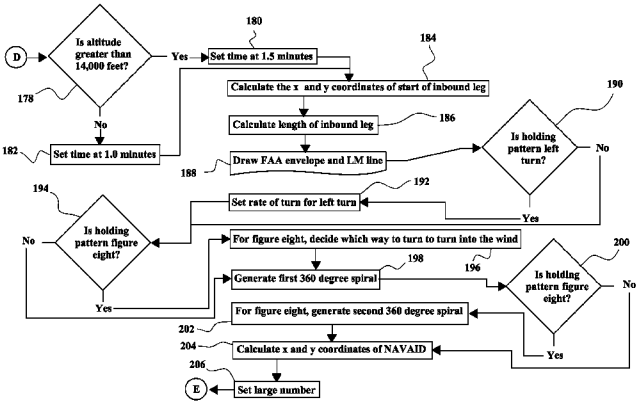
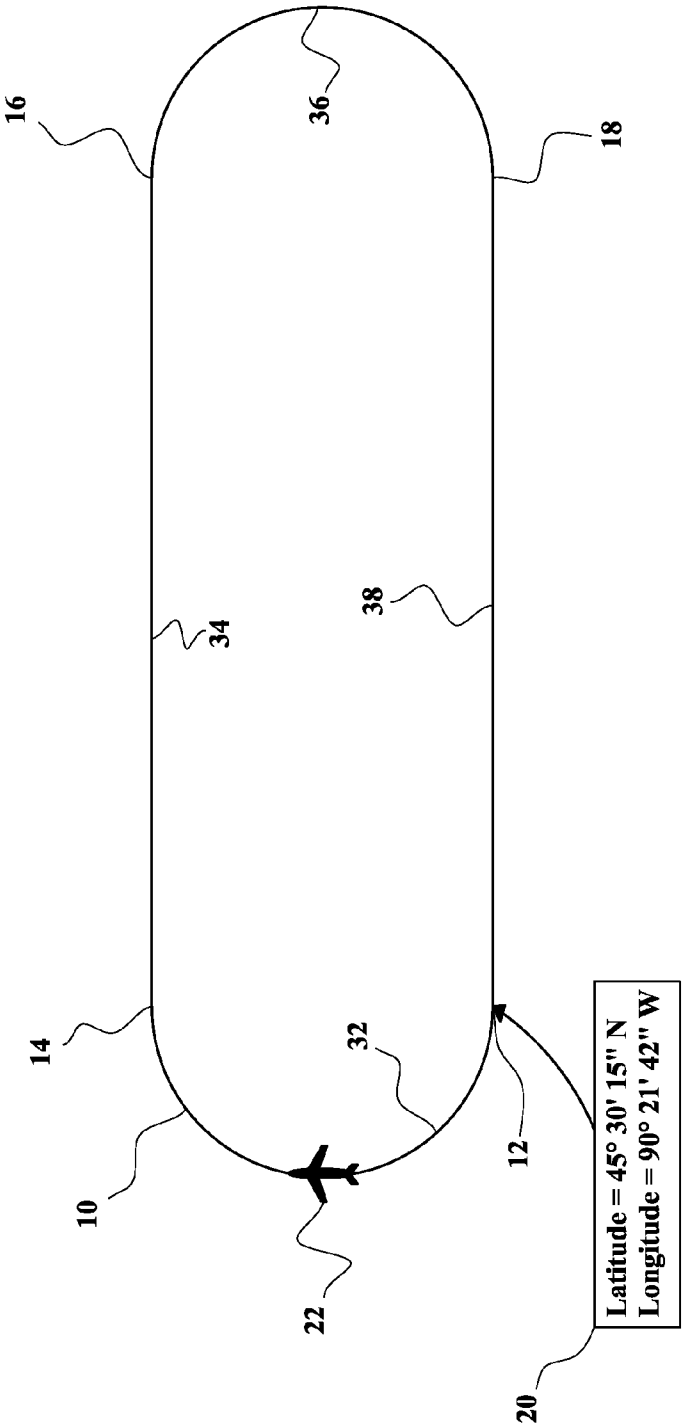
Assistant Examiner — Rebecca Wagner
(74) *Attorney, Agent, or Firm* — Swift & Swift; Stephen Christopher Swift

(57) **ABSTRACT**

A method of calculating Federal Aviation Administration (FAA) published or FAA Air Traffic Control assigned aeronautical holding patterns, comprising the steps of: defining navigational way points using their latitude and longitude coordinates; displaying the latitude and longitude that define the point for an inbound turn; defining four posts of a holding pattern; and showing the actual holding space dimensions along with the non-protected airspace. The method may be performed by a stand-alone electronic device or an electronic device having other functions. The latitude and longitude that define the point for an inbound turn can be displayed as a bearing, and/or as a distance along a radial. The inbound turning point can be calculated using a global positioning or flight management system. A turn may be commanded using an automatic flight control system or flight director. The holding pattern can be drawn to the correct shape with regards wind direction and velocity, or used as an overlay over a representation of terrain.

20 Claims, 23 Drawing Sheets




16
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Latitude = 45° 30' 15" N
Longitude = 90° 21' 42" W
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FIG. 1

FIG. 2

FIG. 3

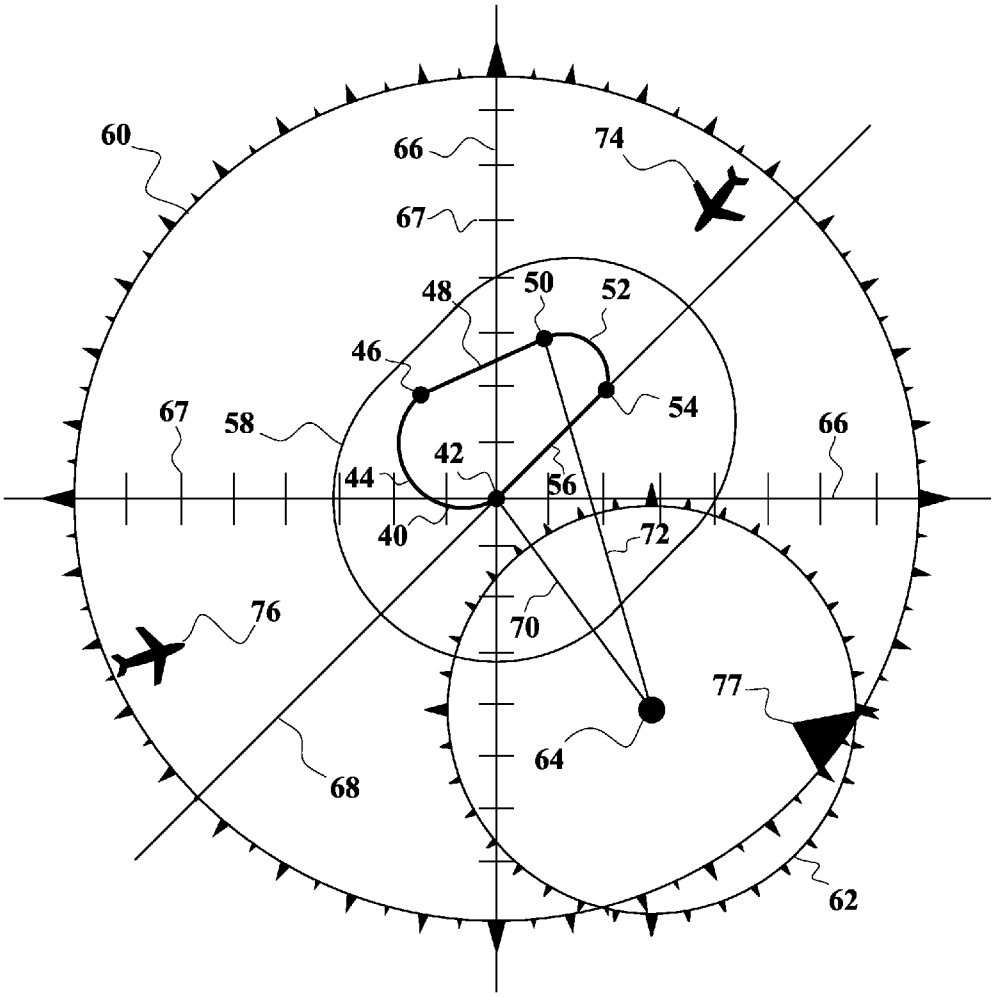


FIG. 4

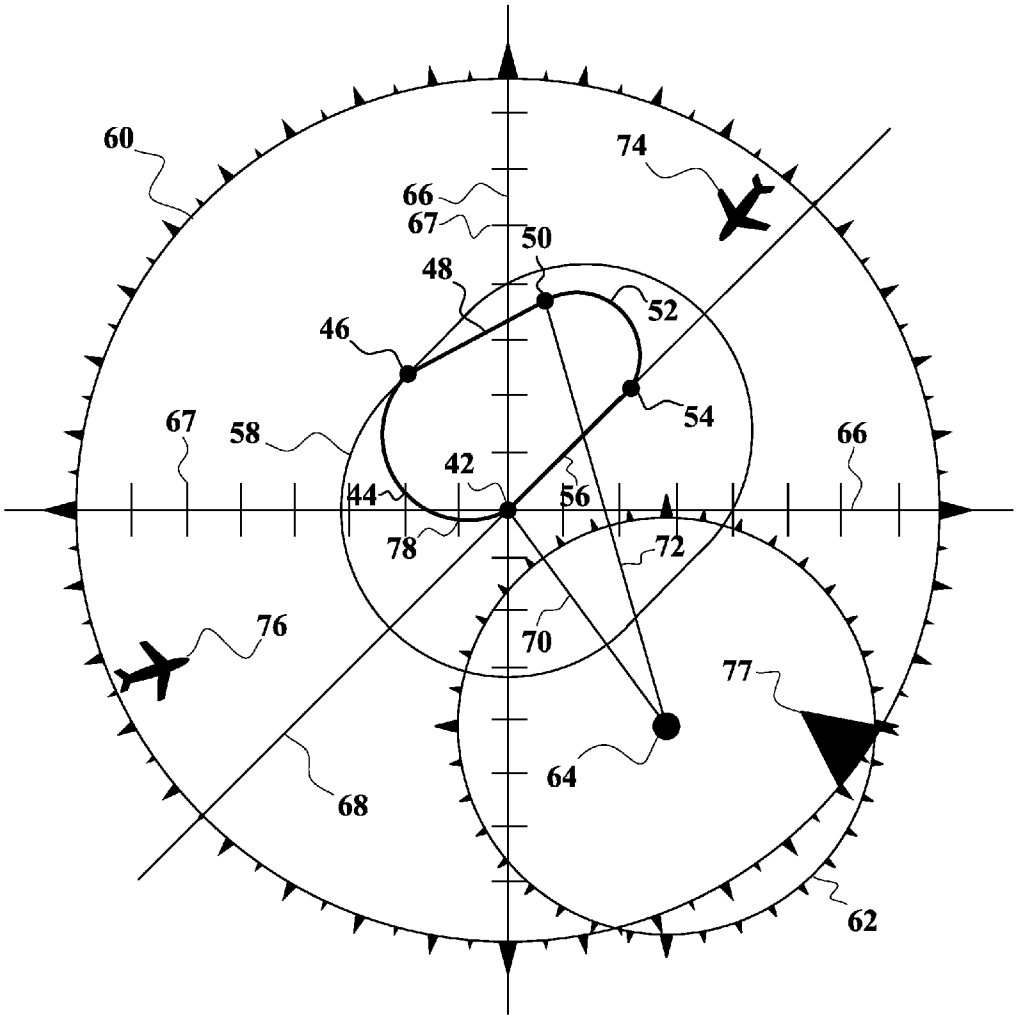


FIG. 5

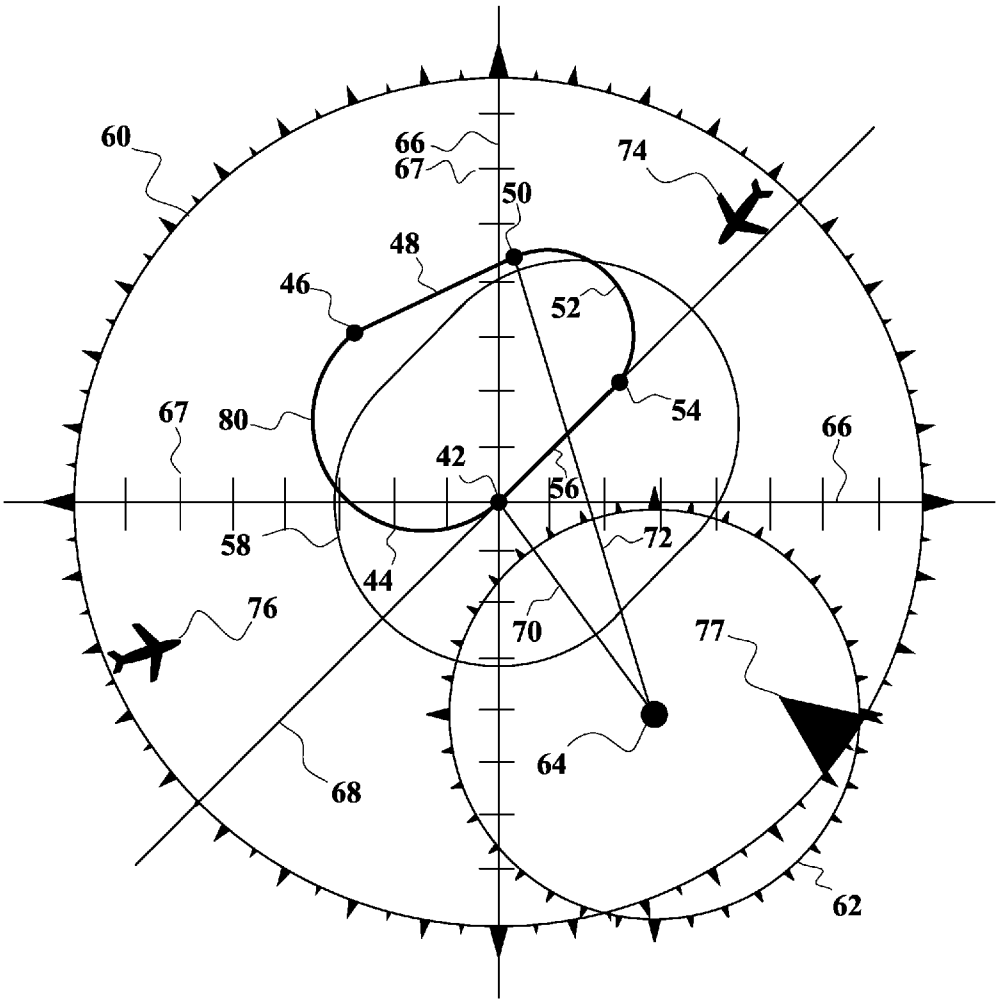
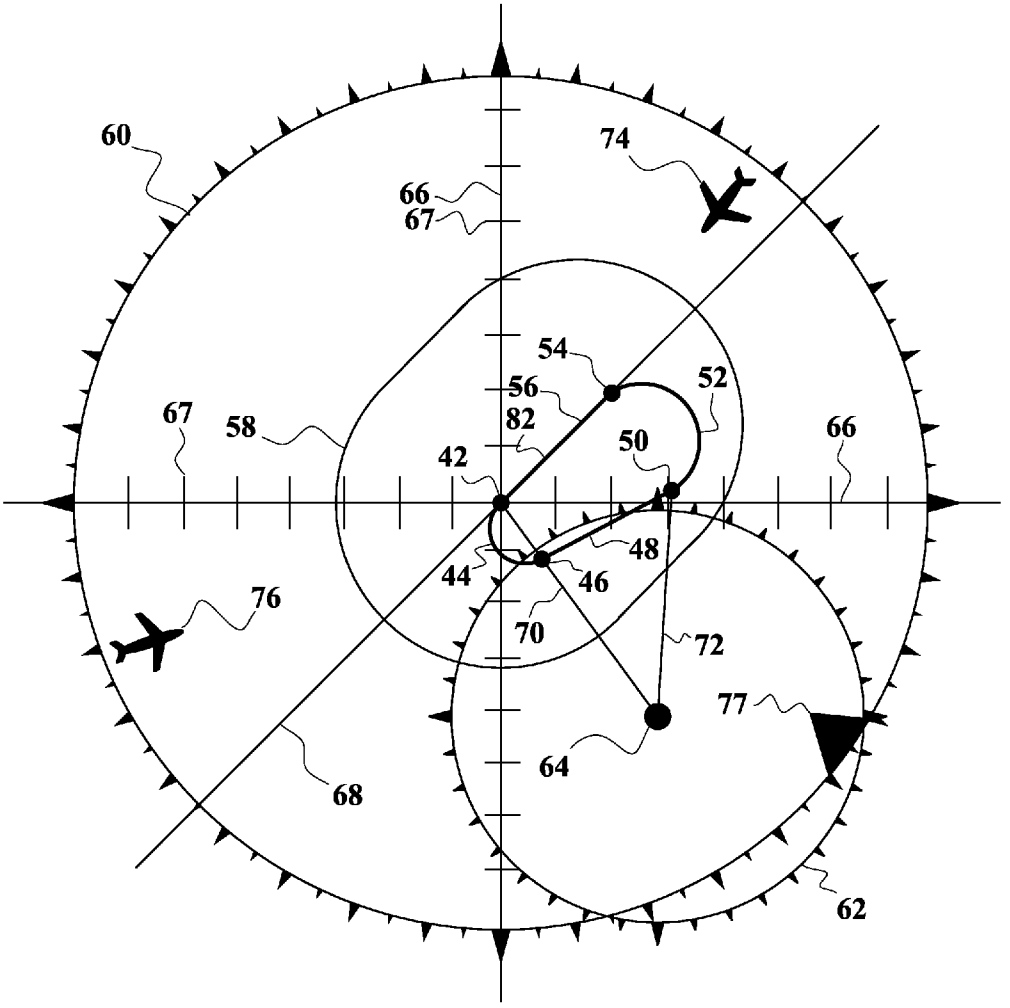


FIG. 6



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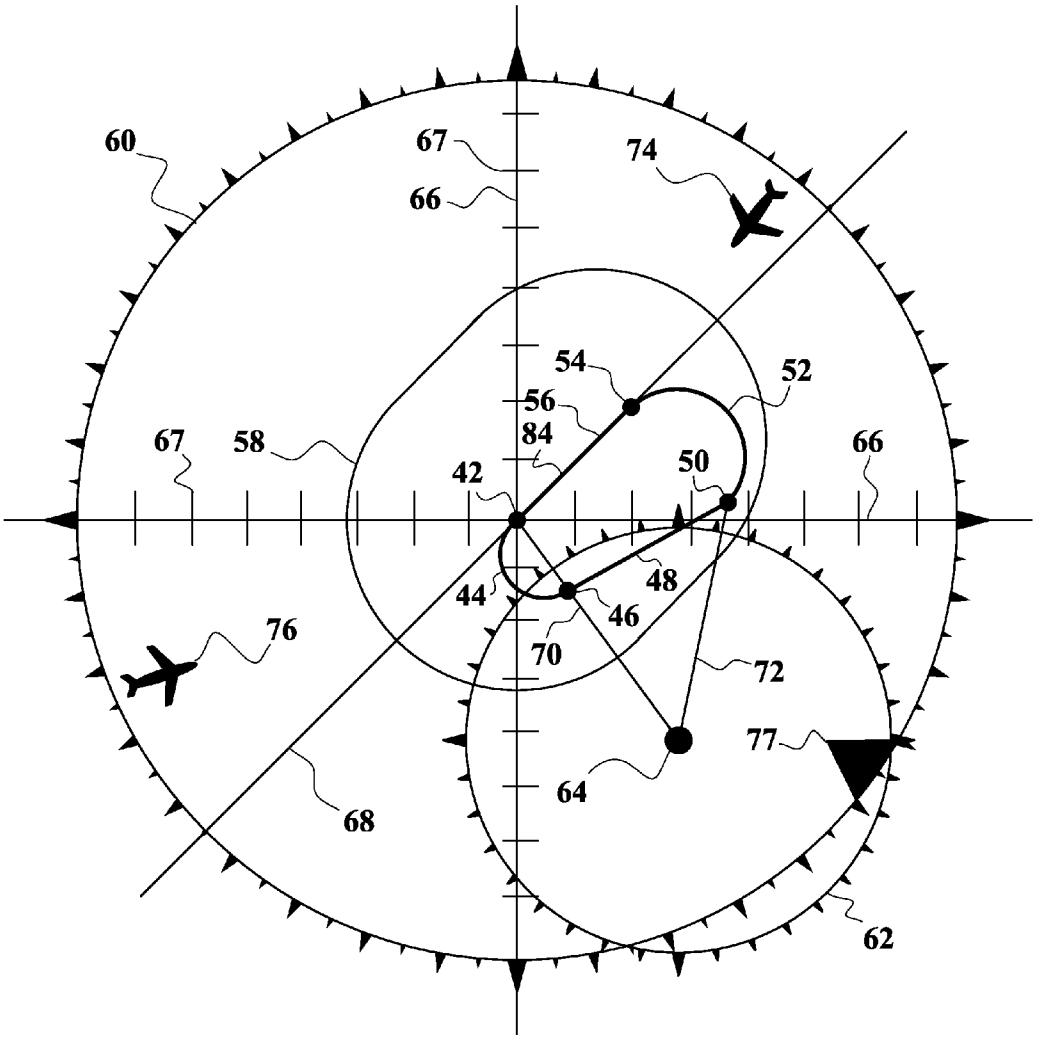
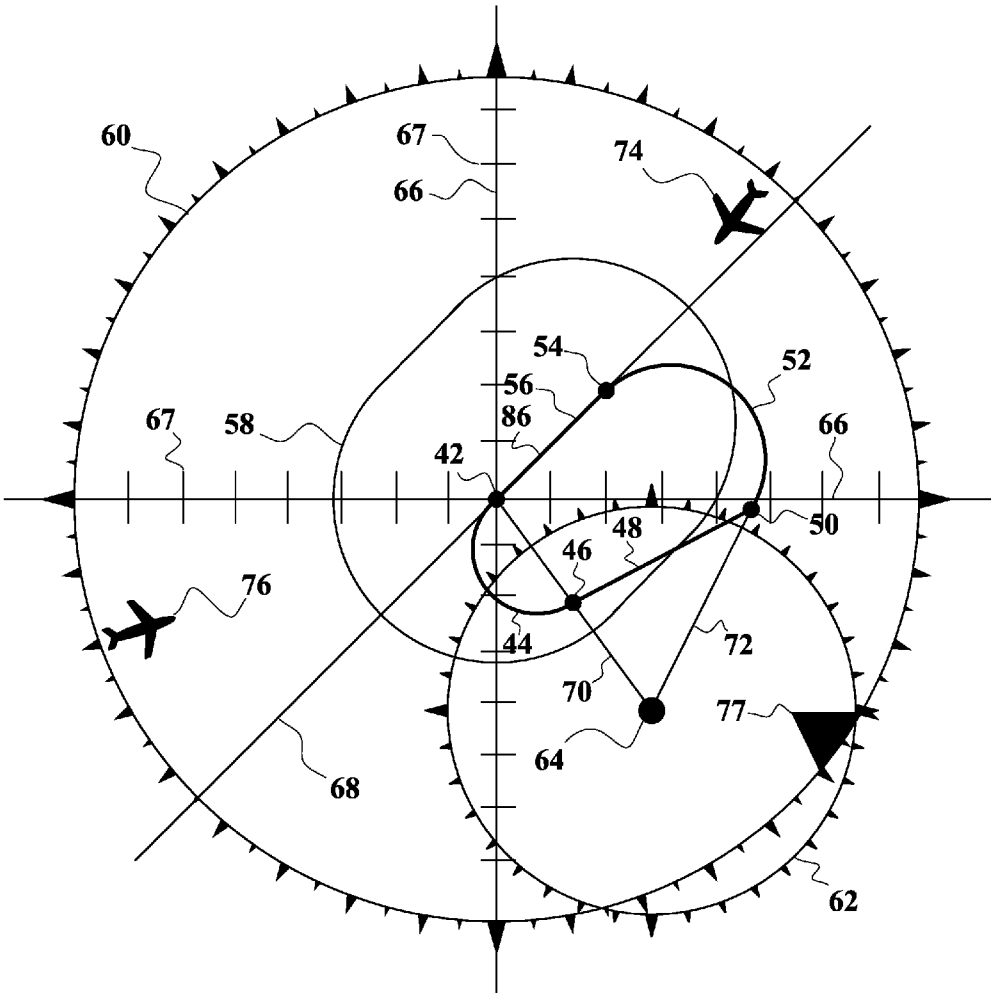


FIG. 8



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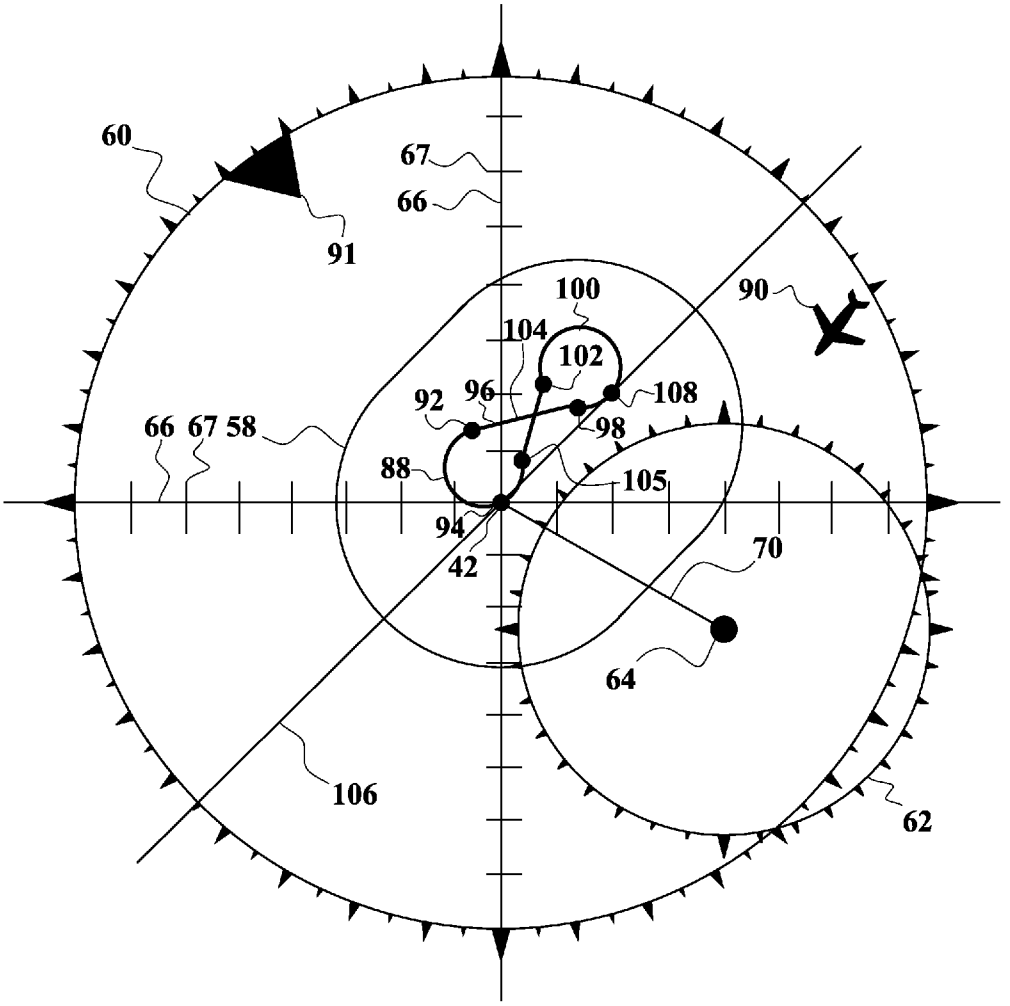
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FIG. 10

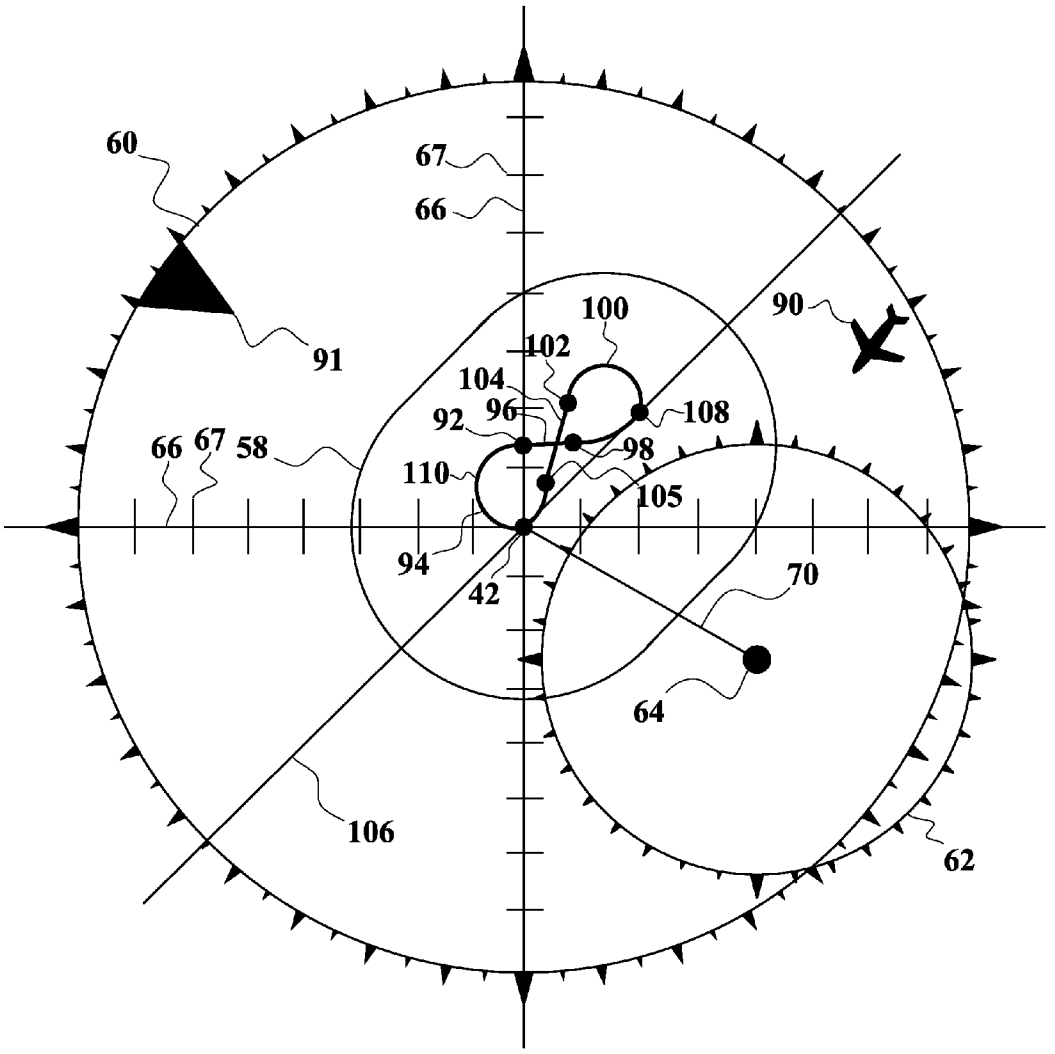
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FIG. 11

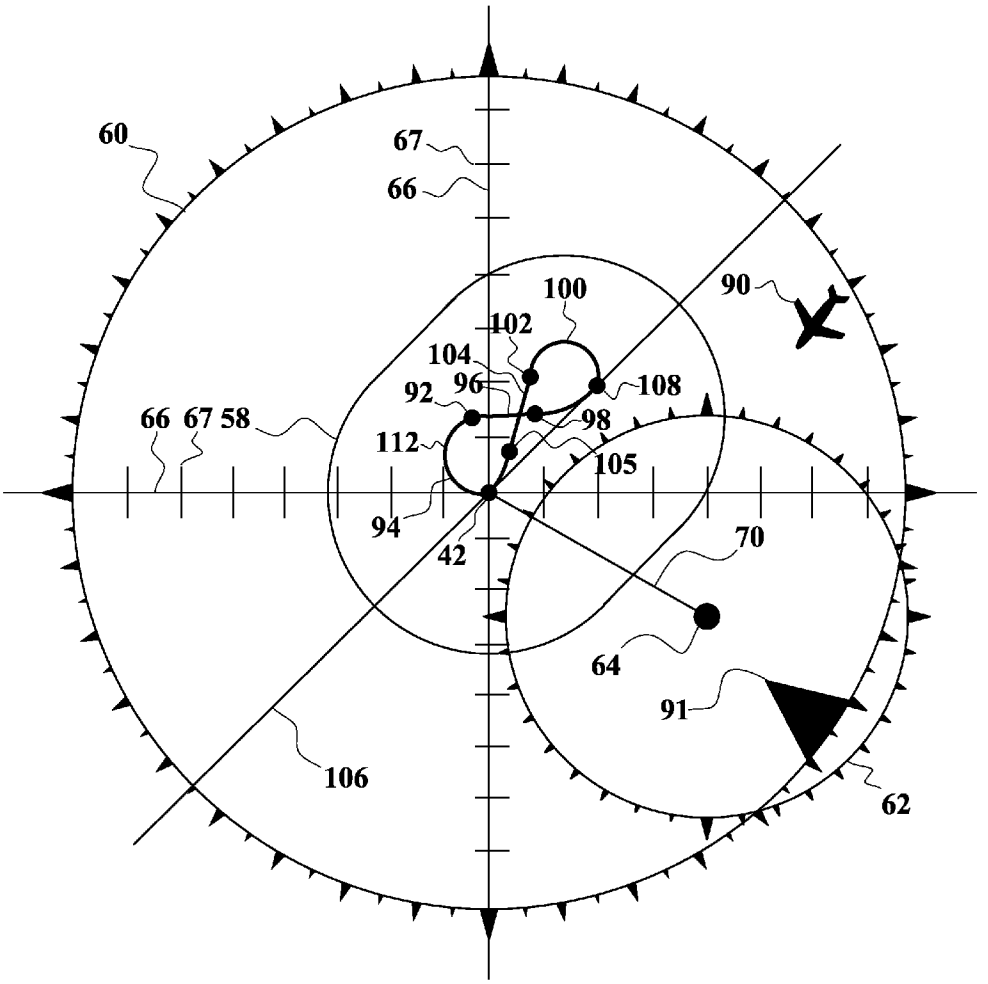
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FIG. 12

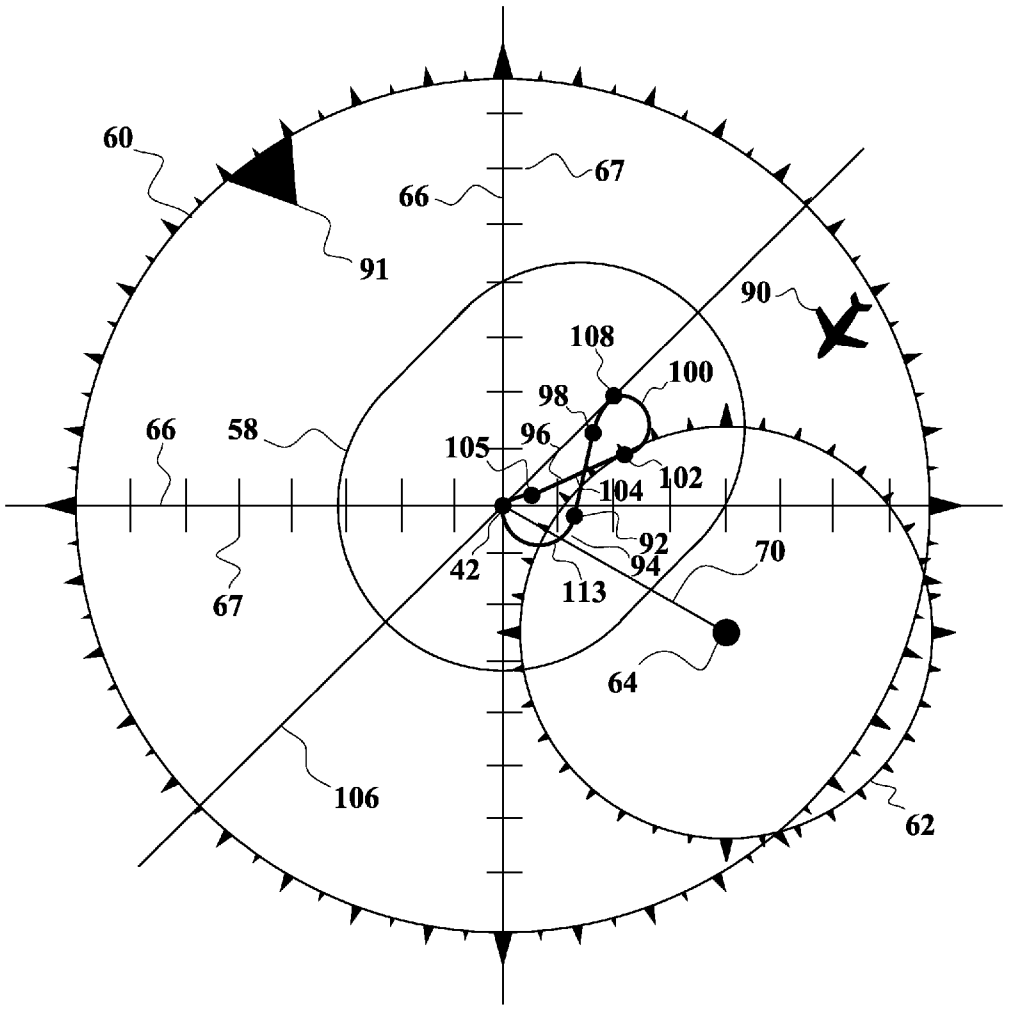
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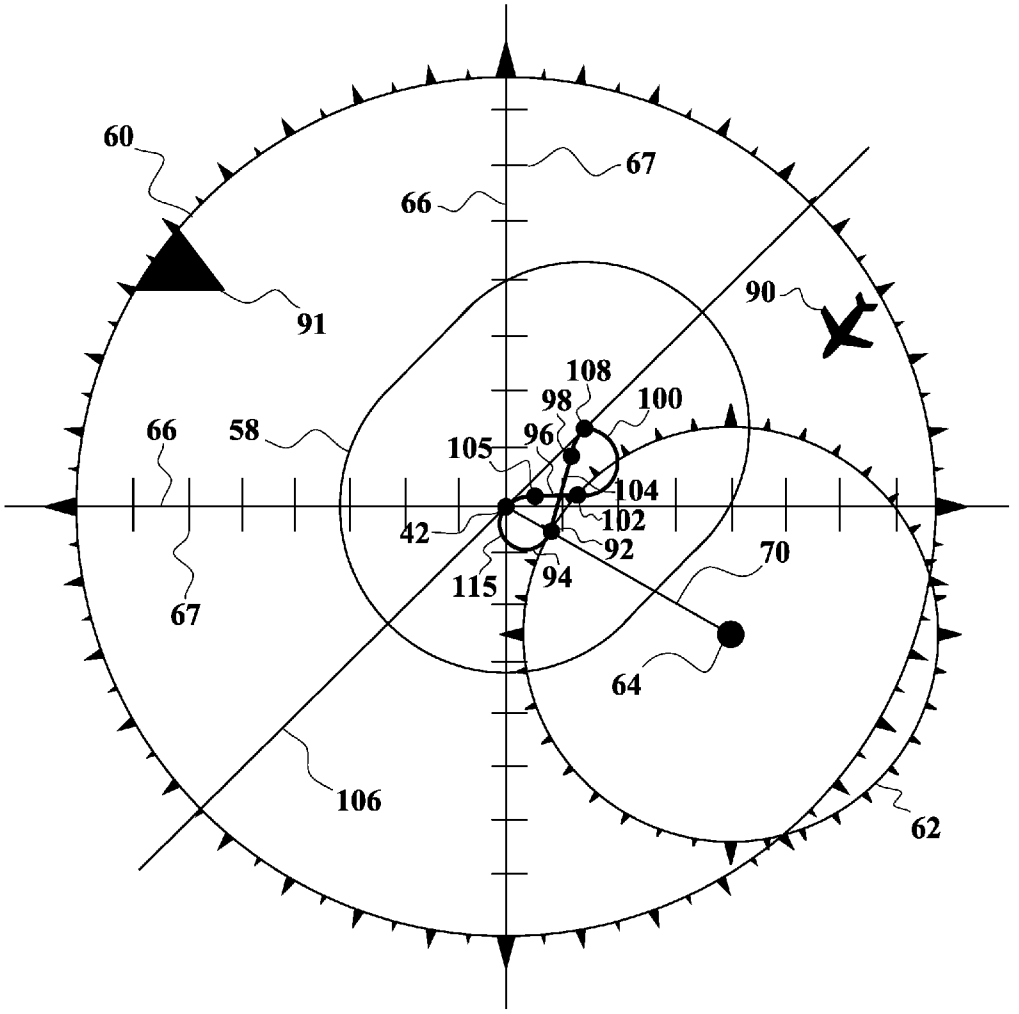
FIG. 13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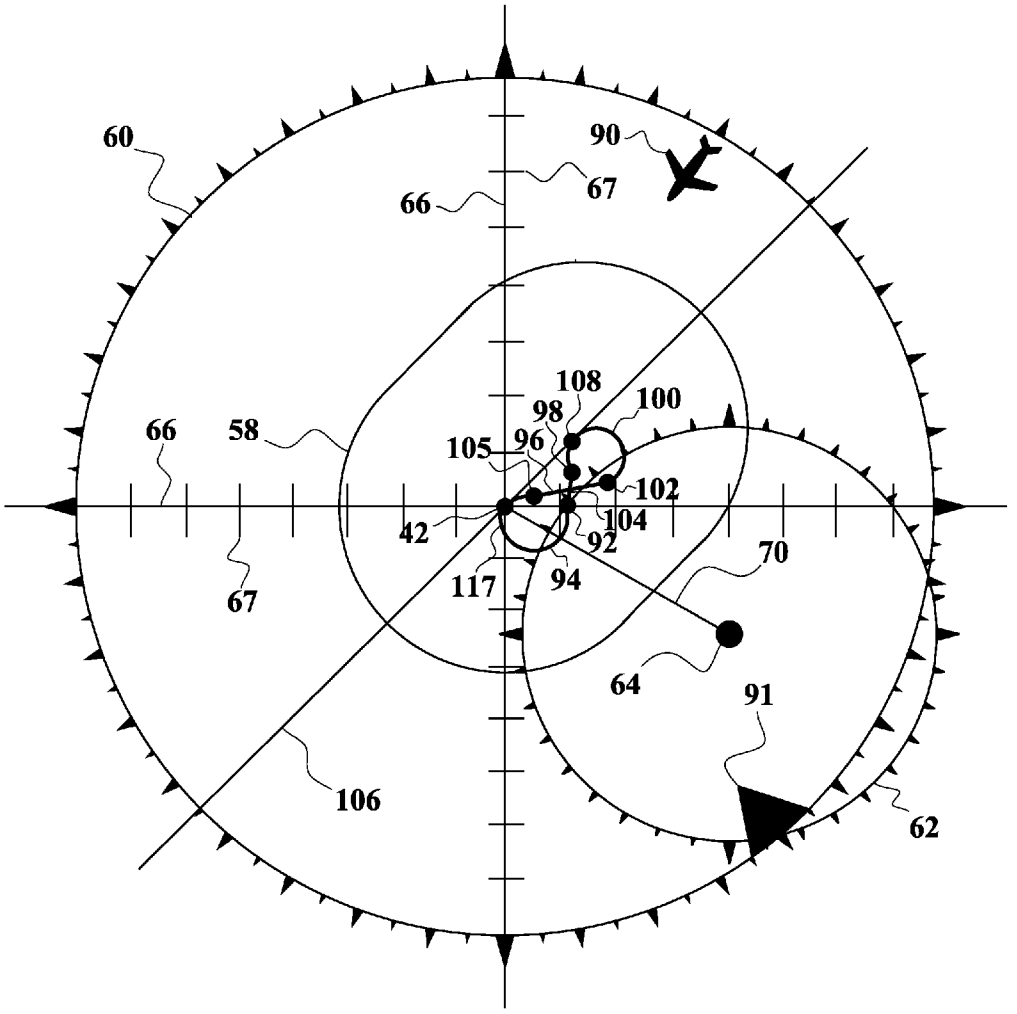
106
62

FIG. 14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106
62

FIG. 15

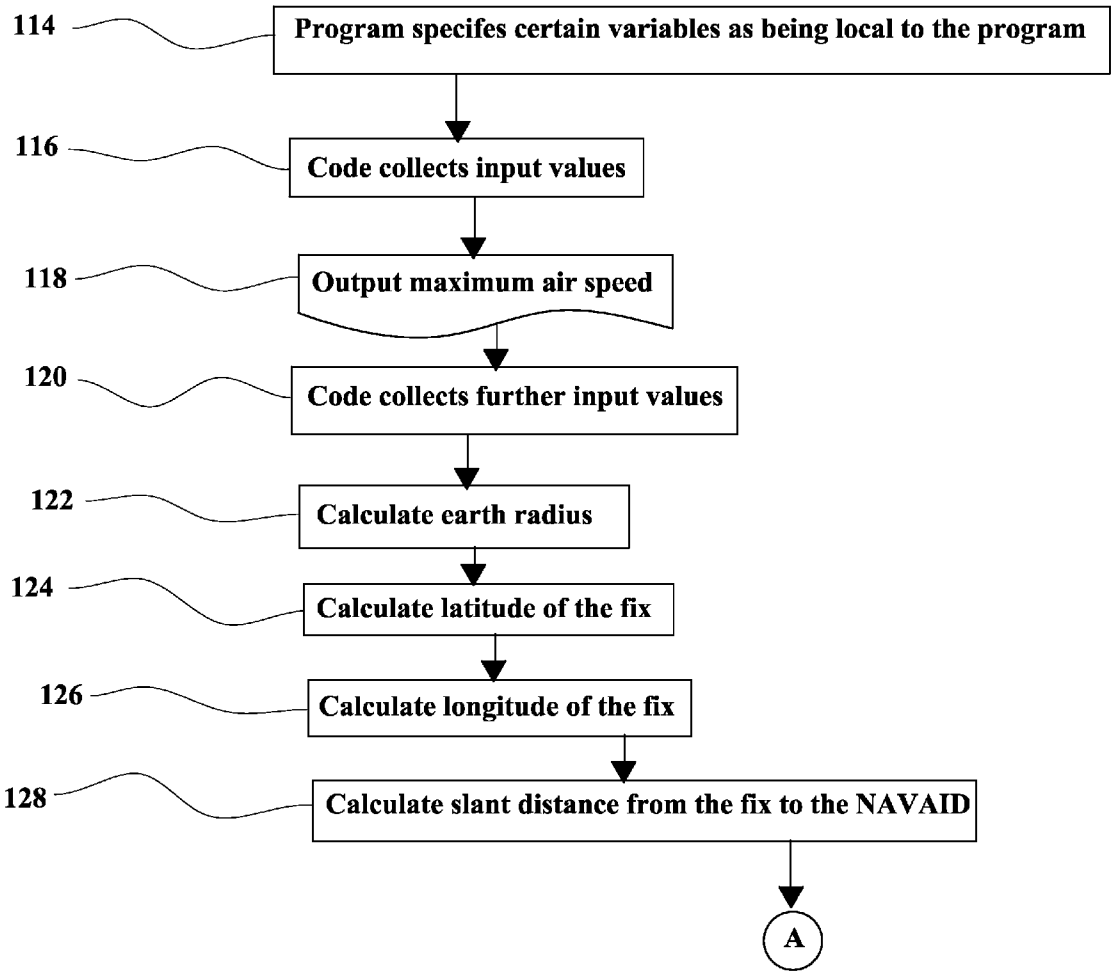
114
Program specifes certain variables as being local to the program
116
Code collects input values
118
Output maximum air speed
120
Code collects further input values
122
Calculate earth radius
124
Calculate latitude of the fix
126
Calculate longitude of the fix
128
Calculate slant distance from the fix to the NAVAID
A

FIG. 16

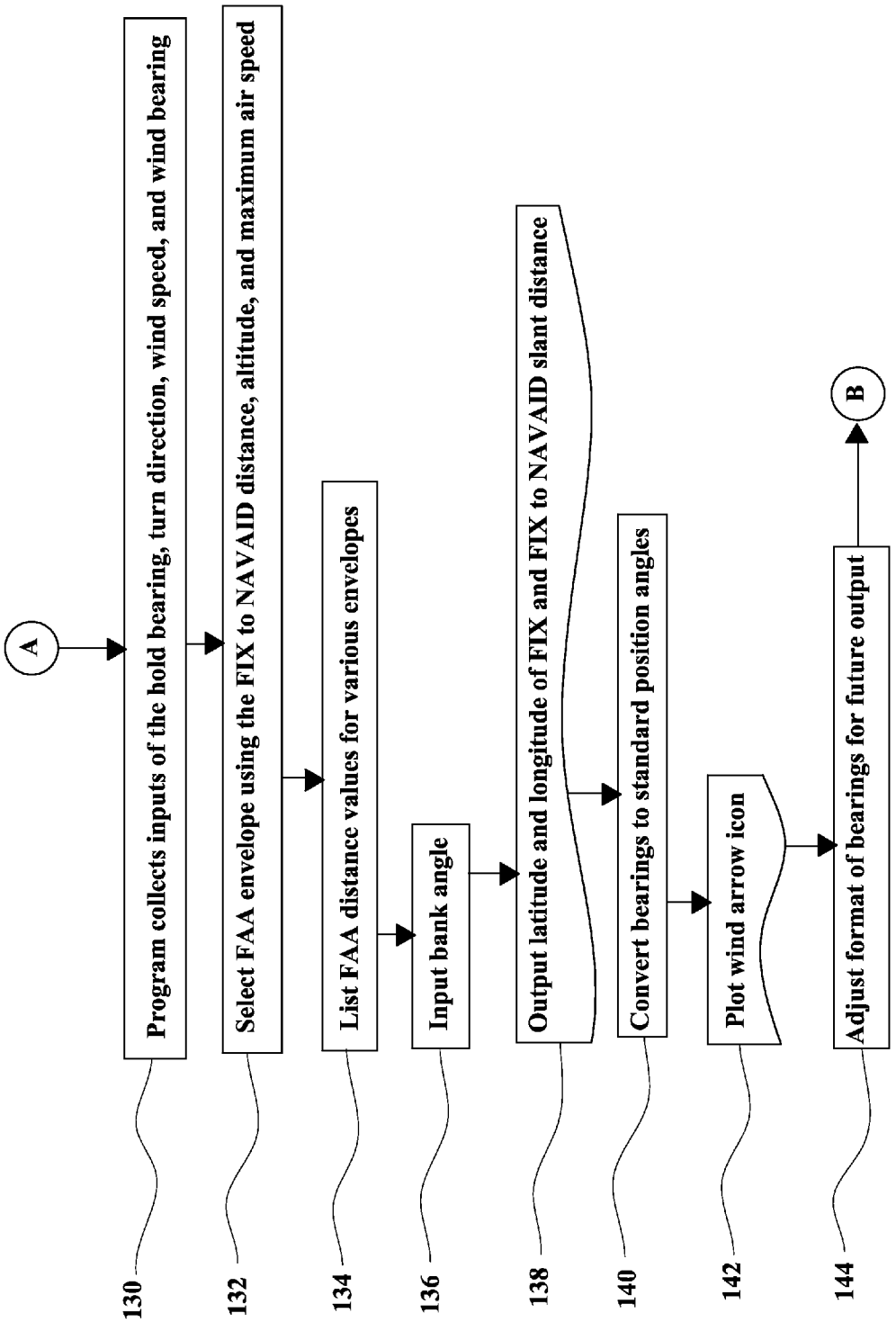
A
Program collects inputs of the hold bearing, turn direction, wind speed, and wind bearing
Select FAA envelope using the FIX to NAVAID distance, altitude, and maximum air speed
List FAA distance values for various envelopes
Input bank angle
Output latitude and longitude of FIX and FIX to NAVAID slant distance
Convert bearings to standard position angles
Plot wind arrow icon
Adjust format of bearings for future output
B
130
132
134
136
138
140
142
144

FIG. 17

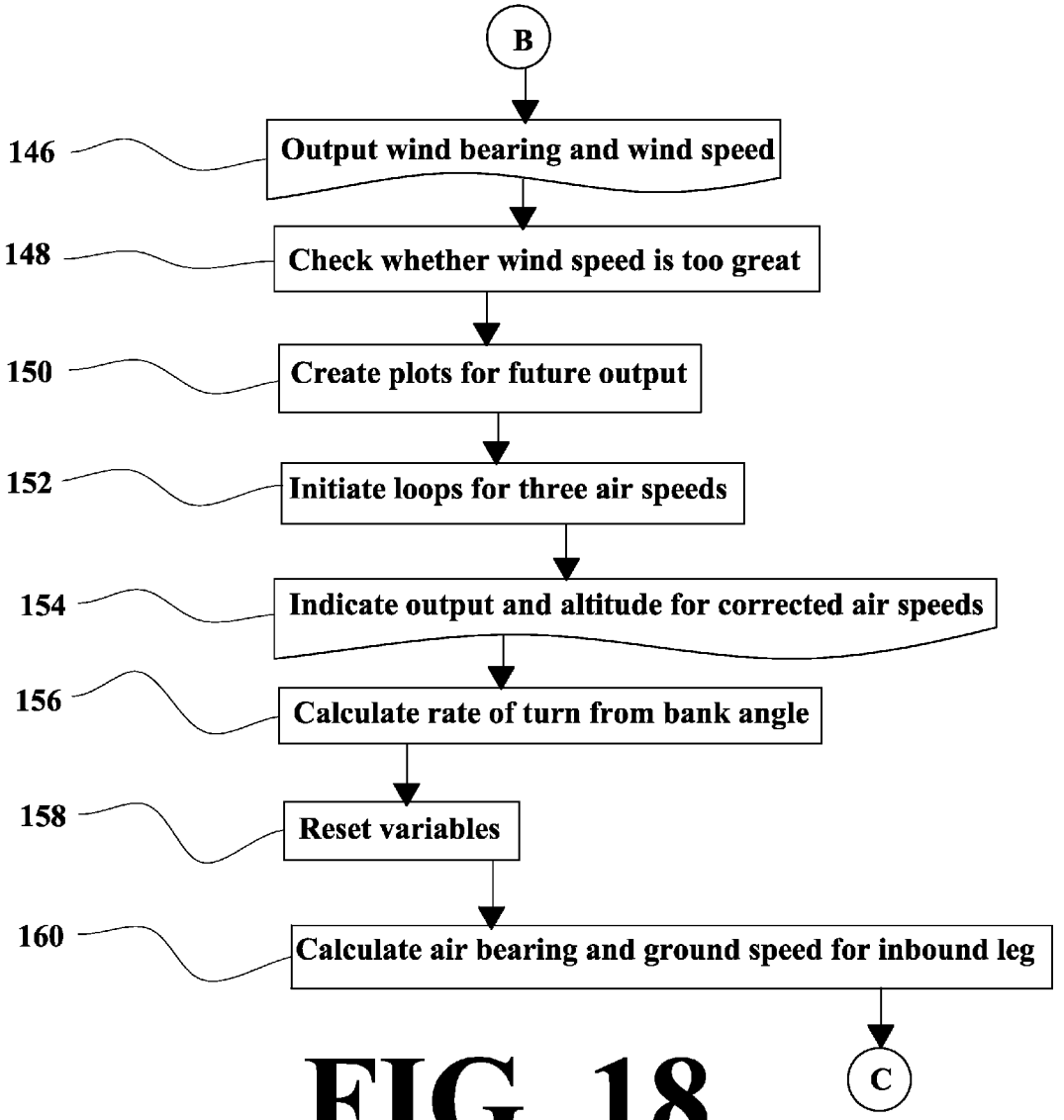
B
146
Output wind bearing and wind speed
148
Check whether wind speed is too great
150
Create plots for future output
152
Initiate loops for three air speeds
154
Indicate output and altitude for corrected air speeds
156
Calculate rate of turn from bank angle
158
Reset variables
160
Calculate air bearing and ground speed for inbound leg
C

FIG. 18

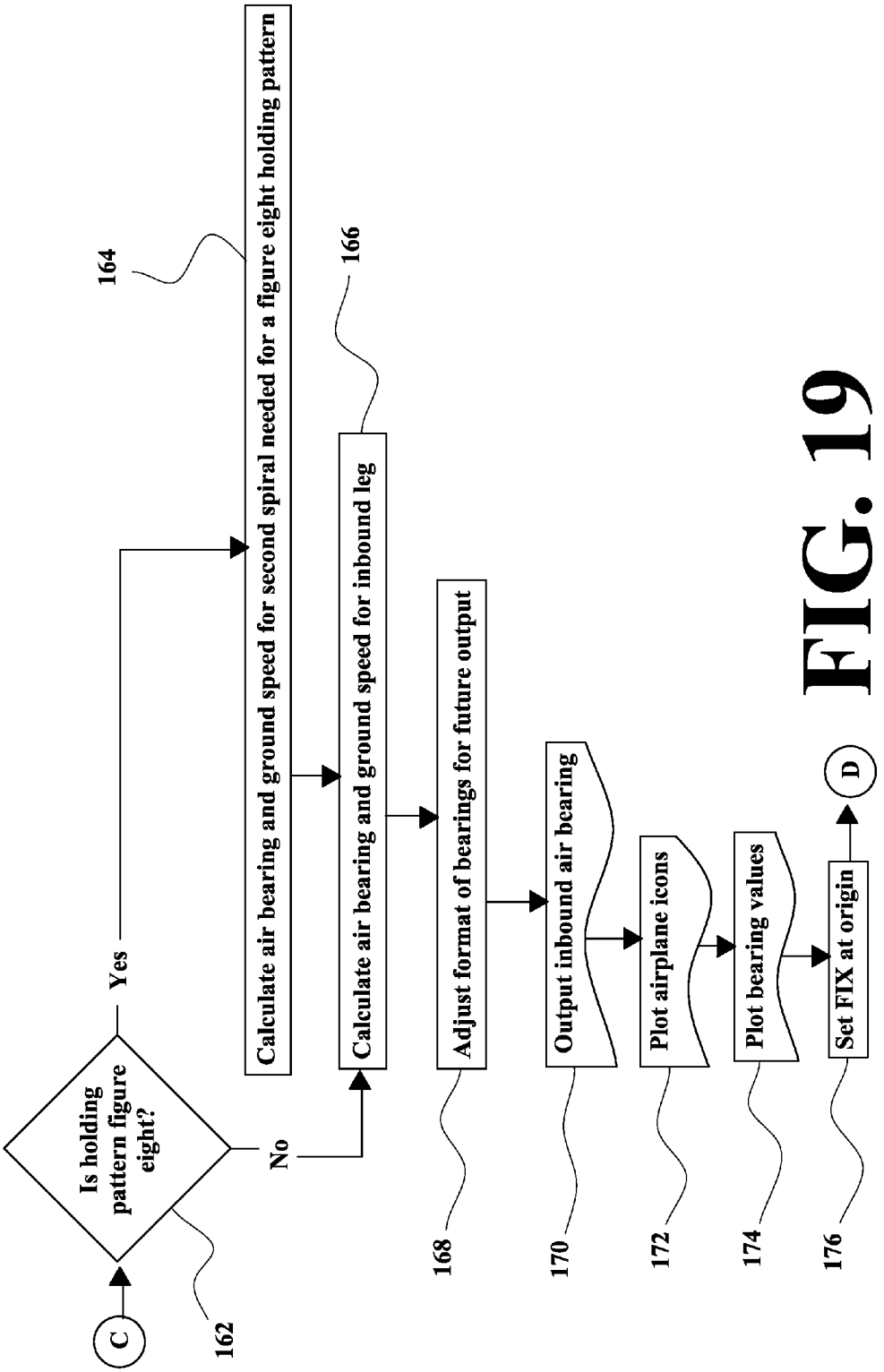
C
Is holding pattern figure eight?
162
Yes
No
164
Calculate air bearing and ground speed for second spiral needed for a figure eight holding pattern
166
Calculate air bearing and ground speed for inbound leg
168
Adjust format of bearings for future output
170
Output inbound air bearing
172
Plot airplane icons
174
Plot bearing values
176
Set FIX at origin
D

FIG. 19

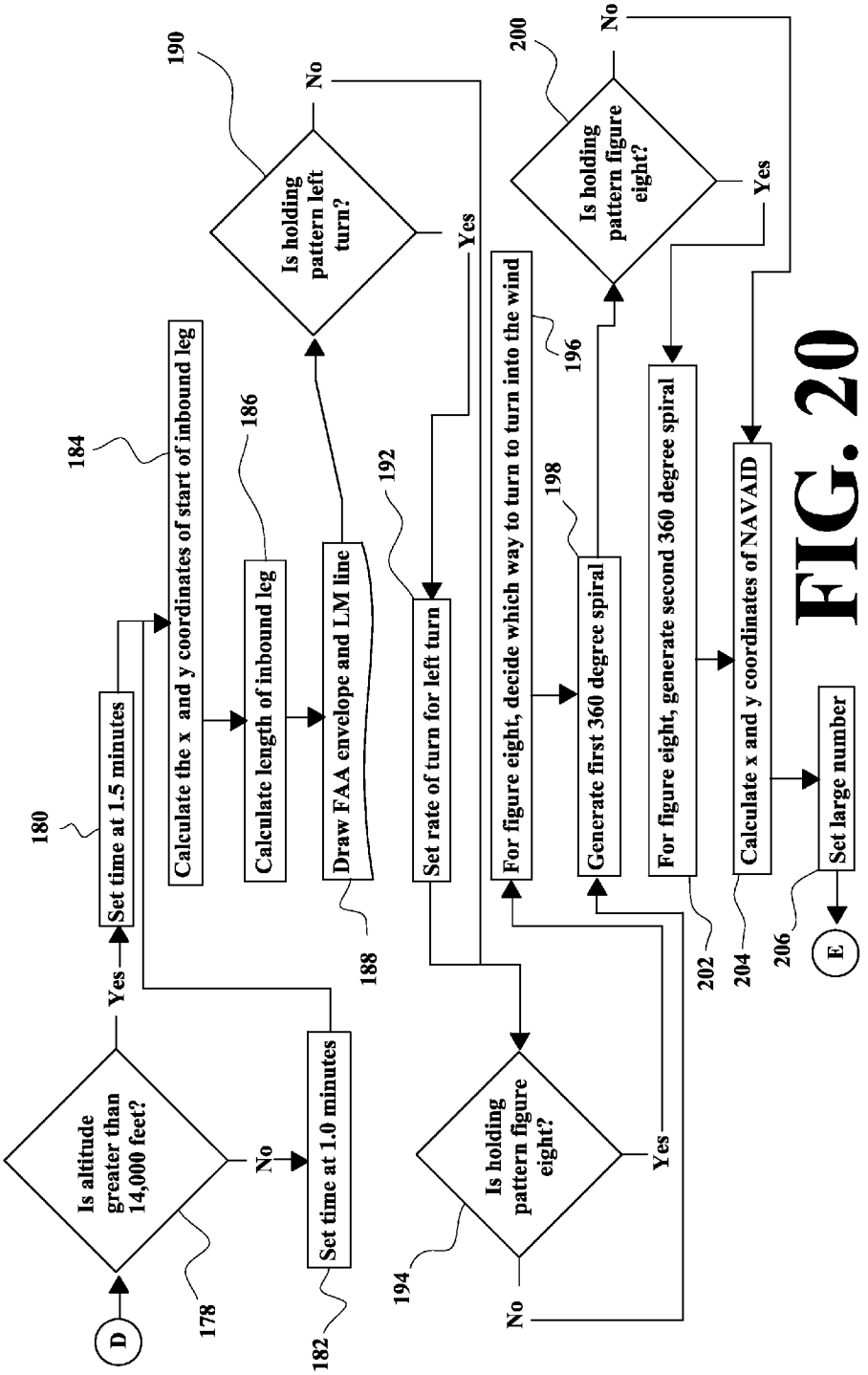
D
Is altitude greater than 14,000 feet?
178
Yes
No
Set time at 1.5 minutes
180
Set time at 1.0 minutes
182
Calculate the x and y coordinates of start of inbound leg
184
Calculate length of inbound leg
186
Draw FAA envelope and LM line
188
Is holding pattern left turn?
190
No
Yes
Set rate of turn for left turn
192
Is holding pattern figure eight?
194
No
Yes
For figure eight, decide which way to turn to turn into the wind
196
Generate first 360 degree spiral
198
Is holding pattern figure eight?
200
No
Yes
For figure eight, generate second 360 degree spiral
202
Calculate x and y coordinates of NAVAID
204
Set large number
206
E

FIG. 20

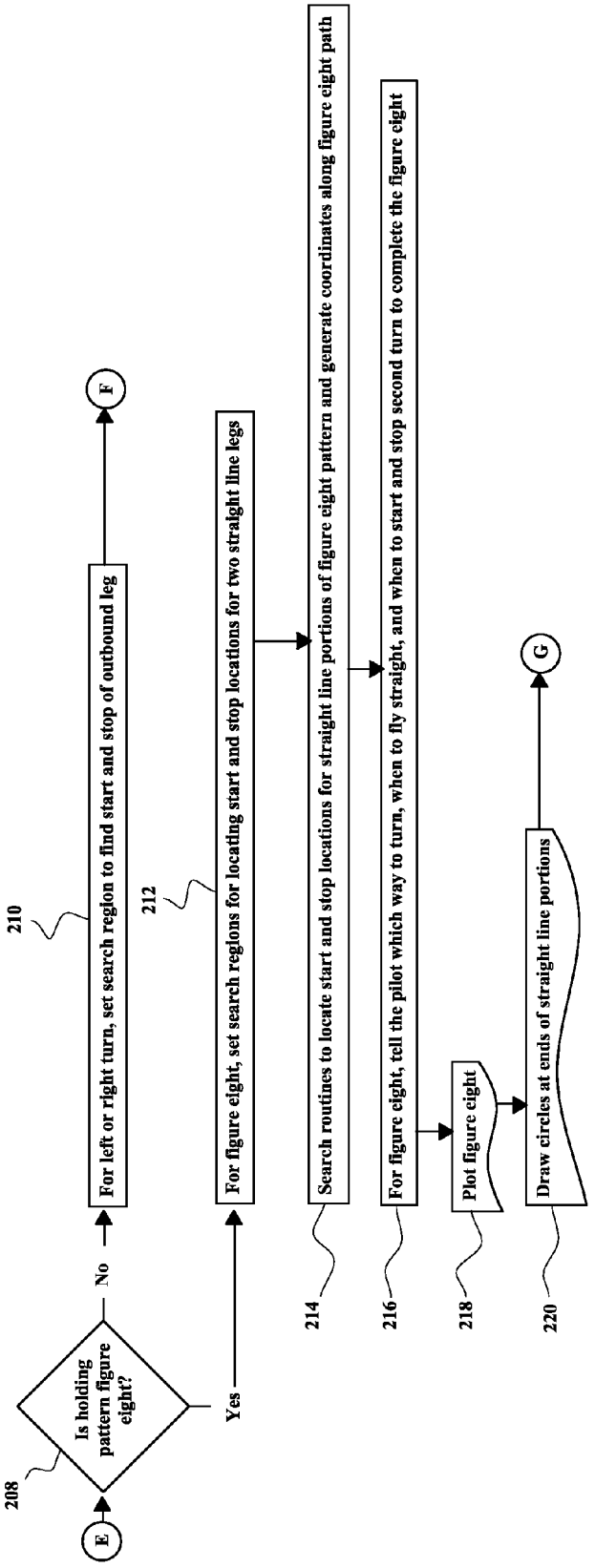
E
208
Is holding pattern figure eight?
No
Yes
210
For left or right turn, set search region to find start and stop of outbound leg
F
212
For figure eight, set search regions for locating start and stop locations for two straight line legs
214
Search routines to locate start and stop locations for straight line portions of figure eight pattern and generate coordinates along figure eight path
216
For figure eight, tell the pilot which way to turn, when to fly straight, and when to start and stop second turn to complete the figure eight
218
Plot figure eight
220
Draw circles at ends of straight line portions
G

FIG. 21

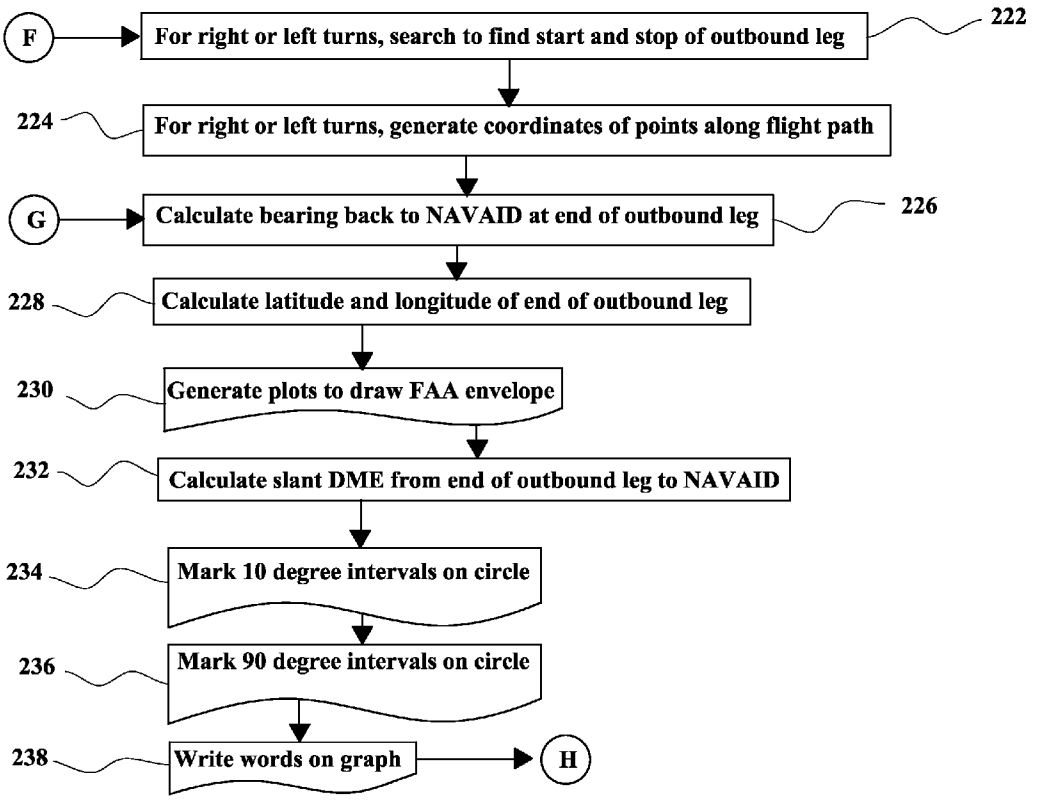
F
For right or left turns, search to find start and stop of outbound leg
222
224
For right or left turns, generate coordinates of points along flight path
G
Calculate bearing back to NAVAID at end of outbound leg
226
228
Calculate latitude and longitude of end of outbound leg
230
Generate plots to draw FAA envelope
232
Calculate slant DME from end of outbound leg to NAVAID
234
Mark 10 degree intervals on circle
236
Mark 90 degree intervals on circle
238
Write words on graph
H

FIG. 22

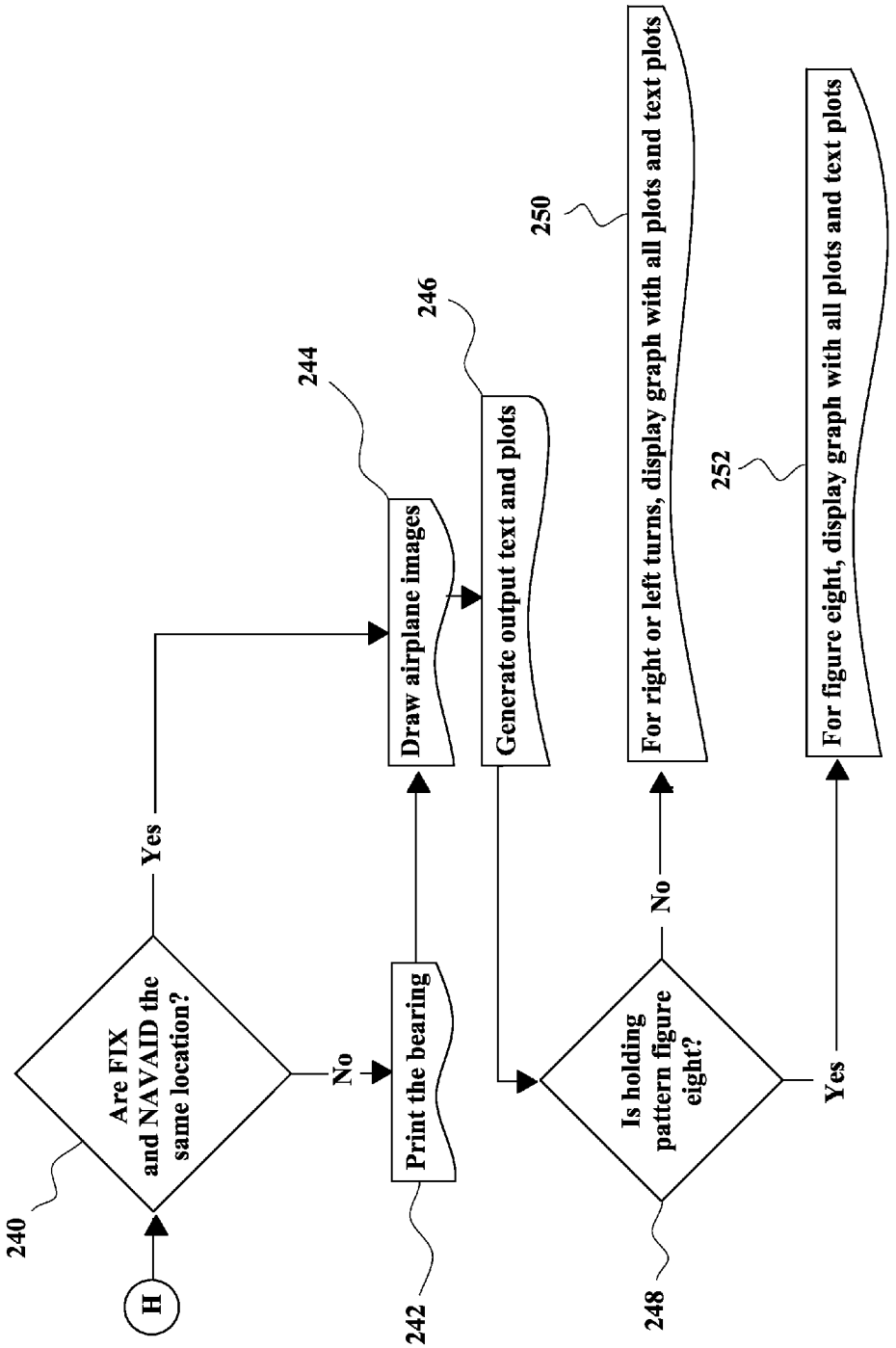
H
240
Are FIX and NAVAID the same location?
Yes
No
Print the bearing
242
Draw airplane images
244
Generate output text and plots
246
Is holding pattern figure eight?
248
No
Yes
For right or left turns, display graph with all plots and text plots
250
For figure eight, display graph with all plots and text plots
252

FIG. 23

AERONAUTICAL HOLDING PATTERN CALCULATION FOR SOLVING HIGH WIND AND PROTECTED AIRSPACE ISSUES

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to improved methods and systems for calculating Federal Aviation Administration (FAA) published or FAA Air Traffic Control assigned aeronautical holding patterns, using electronic devices.

2. Description of the Prior Art

There have been numerous prior inventions for determining holding patterns for aircraft, but none that are equivalent to the present invention.

U.S. Pat. No. 3,110,965, issued on Nov. 19, 1963, to James A. Kittock, discloses a device to aid pilots in entering and maintaining a holding pattern from a preset holding fix. It is not a method using an electronic device, but is an entry calculator (for tear drop, parallel and direct entries), and has no wind corrections, as is the instant invention.

U.S. Pat. No. 4,182,171, issued on Jan. 8, 1980, to Ivan L. Looker, discloses an aircraft navigation device that aids a pilot in flying holding patterns. Although it includes VOR radio receivers, it is not a method using an electronic device, does not calculate a heading, and does not calculate wind corrections, as in the instant invention.

U.S. Pat. No. 4,274,204, issued on Jun. 23, 1981, to Freddy R. Self, discloses an aircraft pattern computer, that is a mechanical device, rather than a method using an electronic device, and is primarily a traffic pattern calculator, not a holding pattern calculator, and does not calculate outbound heading or wind corrections, as does the instant invention.

U.S. Pat. No. 6,167,627, issued on Jan. 2, 2001, to Bruce Gary Wilder and Otto Charles Wilke, discloses an aeronautical holding pattern calculator, having both mechanical and electronic embodiments. It does not disclose the improvements that are the subject of the instant invention, including the use of the differential equations given below.

U.S. Pat. No. 6,678,587, issued on Jan. 13, 2004, to Ronald J. Miller, discloses a system for a tanker plane entering a rendezvous orbit with a plane to be refueled, that includes entering a holding pattern. It does not disclose the use of the differential equations of the instant invention. It is designed for military operations, and for airspace that is designed specifically for an air refueling mission, not for civilian holding patterns, as is the instant invention.

U.S. Pat. No. 6,847,866, issued on Jan. 25, 2005, to Chad E. Gaier, discloses shortened aircraft holding patterns using FMS. It does not disclose the use of the differential equations of the instant invention. It is for exiting a hold, not staying in the hold, and it does not indicate whether you are within the FAA protected airspace, as does the instant invention.

U.S. Pat. No. 7,003,383, issued on Feb. 21, 2006, to Jim R. Rumbo et al., discloses a flight management system using holding pattern entry algorithms. It does not disclose the use of the differential equations of the instant invention. Its algorithms are specifically for hold entries (teardrop, parallel and direct) and it does not account for Federal Aviation Administration (FAA) holding space parameters, as does the instant invention.

U.S. Pat. No. 7,152,332, issued on Dec. 26, 2006, to Ashish Kumar Jain and Gerald Lamar Miley, discloses a navigational assist system for determining entry procedures for holding and runway traffic patterns. It is a simplistic mechanical device, rather than a method using an electronic device as in the instant invention, that calculates outbound headings and wind corrections, and depicts holding space limits.

U.S. Pat. No. 7,370,790, issued on May 13, 2008, to Jan Martincik and Jana Martincikova, discloses an apparatus for visualizing and determining a holding pattern and entry procedure. It is a mechanical device, rather than a method using an electronic device as in the instant invention. It is a visual aid to identify the quadrant the plane is flying in for teardrop, parallel and direct holding pattern entries. It does not correct for wind, nor provide information on an outbound heading or airspace, as does the instant invention.

U.S. Pat. No. 7,903,000, issued on Mar. 8, 2011, to Jason L. Hammack et al., discloses a system for representing a holding pattern on a vertical situation display. It does not disclose the use of the differential equations of the instant invention. It does not show a wind compensated holding pattern and FAA protected airspace, as does the instant invention.

U.S. Pat. No. Des. 377,942, issued on Feb. 11, 1997, to John K. McCloy, discloses a design for a multi-layer rotary holding pattern entry calculator. Again, it is a mechanical device, rather than a method for using an electronic device as in the instant invention. It is for entry information only, not the hold itself. It does no wind or heading calculations, as does the instant invention.

U.S. Patent Application Publication No. 2009/0319100, issued on Dec. 24, 2009, to Nitin Anand Kale and Keshav Rao, discloses systems and methods for defining and rendering a trajectory of an aircraft. It may be used for holding patterns (see the next to the last sentence in paragraph 0049 on page 7). Again, it does not disclose the use of the differential equations of the instant invention. It may re-label a way point as a holding way point. It does not calculate holding patterns to stay within depicted FAA holding airspace, as does the instant invention.

Japanese Patent No. 7-104853, published on Apr. 21, 1995, inventors Takashi Oki, Masahiro Hattori and Naoyuki Yamashita, discloses an automatically guided flight system for an airplane, capable of following an airplane in a turning course while holding a turning radius. It does not appear to be designed to calculate holding patterns, as in the instant invention.

None of the above inventions and patents, taken either singly or in combination, is seen to describe the instant invention as claimed.

SUMMARY OF THE INVENTION

The present invention is a method of calculating aeronautical holding patterns, that can be used with any aircraft or combination of instruments that can define a bearing, comprising the steps of: defining navigational way points using their latitude and longitude coordinates; displaying the latitude and longitude that define the point for an inbound turn; defining four posts of a holding pattern; showing the actual holding space dimensions along with the non-protected airspace; and determining the necessity for a figure eight holding pattern. The method may be performed by a stand-alone electronic device or an aircraft equipped electronic device having other functions. The latitude and longitude that define the point for an inbound turn can be displayed as a bearing, as a distance along a bearing, or both. The inbound turning point can be incorporated into and automatically calculated using a global positioning system or flight management system. A turn may be commanded using an automatic flight control system or a flight director. The holding pattern can be drawn to the correct shape with regards to wind direction and velocity, or used as an overlay over a representation of terrain.

Accordingly, it is a principal object of the invention to further simplify the process of flying an airplane or other aerial vehicle in a holding pattern.

It is another object of the invention to improve air safety by enabling pilots to fly holding patterns more accurately and with less distraction.

It is a further object of the invention to prevent unnecessary fuel consumption from errors in flying holding patterns.

Still another object of the invention is to provide methods that will be useful in training new pilots to fly holding patterns.

It is an object of the invention to provide improved elements and arrangements thereof in an apparatus for the purposes described which is cost effective, dependable and fully effective in accomplishing its intended purposes.

These and other objects of the present invention will become readily apparent upon further review of the following specification and drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is graphical representation of a holding pattern using the invention.

FIG. **2** is graphical representation of a warning regarding flight speed given by the invention.

FIG. **3** is a graphical representation of a warning regarding wind speed given by the invention.

FIG. **4** is a graphical representation of a first right hand holding pattern generated using the invention.

FIG. **5** is a graphical representation of a second right hand holding pattern generated using the invention.

FIG. **6** is a graphical representation of a third right hand holding pattern generated using the invention.

FIG. **7** is a graphical representation of a first left hand holding pattern generated using the invention.

FIG. **8** is a graphical representation of a second left hand holding pattern generated using the invention.

FIG. **9** is a graphical representation of a third left hand holding pattern generated using the invention.

FIG. **10** is a graphical representation of a first figure eight holding pattern generated using the invention.

FIG. **11** is a graphical representation of a second figure eight holding pattern generated using the invention.

FIG. **12** is a graphical representation of a third figure eight holding pattern generated using the invention.

FIG. **13** is a graphical representation of a fourth figure eight holding pattern generated using the invention.

FIG. **14** is a graphical representation of a fifth figure eight holding pattern generated using the invention.

FIG. **15** is a graphical representation of a sixth figure eight holding pattern generated using the invention.

FIG. **16** is a first flow chart showing how the invention may be implemented using a computer program.

FIG. **17** is a second flow chart showing how the invention may be implemented using a computer program.

FIG. **18** is a third flow chart showing how the invention may be implemented using a computer program.

FIG. **19** is a fourth flow chart showing how the invention may be implemented using a computer program.

FIG. **20** is a fifth flow chart showing how the invention may be implemented using a computer program.

FIG. **21** is a sixth flow chart showing how the invention may be implemented using a computer program.

FIG. **22** is a seventh flow chart showing how the invention may be implemented using a computer program.

FIG. **23** is an eighth flow chart showing how the invention may be implemented using a computer program.

Similar reference characters denote corresponding features consistently throughout the attached drawings.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is a calculator (or calculation method) that may be used as (or with) a stand alone electronic device or linked (or used) with a smart phone, IPAD, tablet or laptop computer, flight management system ("FMS") or any other digital electronic media used in aircraft or unmanned aerial vehicle ("UAV") navigation or flight planning.

All navigational way points such as global positioning system ("GPS"), user defined way points, VOR (Very high frequency Omnidirectional Range), VOR/VOR, VOR/DME (Distance Measuring Equipment), TACAN (TACtical Air Navigation), NDB (NonDirectional radio Beacon), NDB/VOR and Marker Beacons will be defined using their latitude and longitude coordinates. The latitude and longitude that define the point for the turn inbound may be displayed as a bearing **20** (shown in FIG. **1**) or distance along a radial, or both.

A bearing may be identified using VOR needles, HSI (Horizontal Situation Indicator) needles, ADF (Automatic Direction Finder) needles, or FMS bearing pointers. Additionally, the FMS or GPS will automatically calculate the turning point inbound based on the mentioned navigation algorithms and procedures. It will then command a turn, based on the same algorithms, through the Automatic Flight Control System ("AFCS" or "autopilot") or Flight Director if flown manually (at the standard rate or as limited by the manufacturer—usually 25 to 30 degrees) to remain in the protected airspace and roll out on the correct inbound course.

A NAVAID (short for navigation aid) is any visual or electronic device, airborne or on the surface, which provides point-to-point guidance information or position data to aircraft in flight. NAVAIDs send out radio signals that an airplane's tuned receiver picks up. The signals may then be tracked using radials or bearings. A waypoint is a reference point in physical space used for navigation. It can be a VOR or GPS identified point. All have longitude and latitude identifiable positions along with a name.

The inbound leg is a straight line path of flight, of one to one and a half minutes duration, that ends at a position called the fix. As the airplane passes over the fix, the pilot begins the outbound turn by banking the plane to a bank angle. As the plane approaches a specified outbound heading, the pilot levels the plane and flies on that heading until the bearing back to the NAVAID is a specified value. He then banks the plane to the same bank angle as before, beginning the inbound turn and continues that turn until the plane reaches the start of the inbound leg. The pilot then levels the wings and uses a defined wind corrected heading to fly the inbound course to the fix and repeats the entire process, until given instructions to proceed from the hold.

The four posts of a holding pattern are the four positions at which changes in flight are made; they are the end of the inbound leg, the end of the outbound turn, the end of the outbound leg, and the beginning of the inbound leg. The holding fix is the only identifiable post in timed holding. Timing of the outbound leg starts abeam the fix or when the wings are level after the turn, whichever comes later. Timing of the inbound leg starts with wings level. The end of the outbound leg is identified using a bearing, or DME along a radial.

The four posts of a holding pattern will be defined onto the depicted, wind corrected holding pattern selected. The actual

holding space dimensions will be viewable in relation to the hold and non-protected airspace. FIG. **1** shows a holding pattern **10**, with the four posts **12**, **14**, **16** and **18**, the inbound turn **32** between **12** and **14**, the inbound leg **34** between **14** and **16**, the outbound turn **36** between **16** and **18**, and the outbound leg **38** between **18** and **12**.

The holding pattern will be drawn to the correct shape with regards to the prevailing winds (defined by wind direction and velocity). This shape will be represented within the protected holding pattern airspace. This pictorial display may also be used as an overlay to show the pilot actual representation of terrain associated with the hold. A moving target **22** representing the aircraft (shown in FIG. **1**) will also be displayed showing the pilot the aircraft's position throughout the hold.

Variable airspeeds will be used with the wind calculations to maintain the aircraft within the protected airspace. Standard FAA (Federal Aviation Administration), ICAO (International Civil Aeronautics Organization), military holding airspeeds, and altitudes will be applied during the calculations of algorithms. With a given bank angle, and starting from the maximum airspeed for a given altitude, three patterns will be displayed. The airspeed for the first pattern will indicate the maximum holding airspeed for that altitude. The second pattern will indicate the maximum airspeed minus 15%, and the third pattern will indicate maximum airspeed minus 30%. The variable airspeed will solve the problem of wind speed to aircraft speed, being outside of a defined workable solution where the wind speeds are equal to 25% or more of the aircraft's speed. If the aircraft is flying too fast or the wind speeds are too great to remain within the protected holding airspace, a message will be generated to notify the pilot that the aircraft will not remain inside the protected airspace. FIG. **2** shows a screen **24** on which a warning regarding flight speed **28** is displayed. A speaker **26** may also give an audible warning **26**. FIG. **3** shows a warning regarding wind speed **30**. For aircraft utilizing an FMS, current information will be taken from the aircraft's onboard computers and sensors and applied to the aircraft's current position.

The FAA has specified the extents and shapes of areas the plane must remain within to be within the holding space dimensions. These envelopes vary with altitude and air speed and are constructed using compasses and rulers. There are many such envelopes. In our program, we have simplified the shape to two straight lines and two semi-circles. If a plane remains within our envelope, it will also be inside the FAA envelope for that altitude and speed. If a plane is outside the FAA envelope, it is in non-protected airspace.

Maximum allowed holding pattern airspeeds will be as specified in Holding Pattern Criteria, paragraphs 2-8.a or 2-8.b, as applicable, pursuant to FAA Order 7130.3A, including all modifying FAA Memoranda, or its successor regulations. Use Table 1: Maximum Holding Airspeeds, page 2-2, FAA Order 7130.3A, including all modifying FAA Memoranda, or its successor regulations, with the "airplane type" input (described below) to identify the maximum allowed holding pattern airspeed. Use Table 2: Holding Pattern Selection Chart, pages 2-3 through 2-5, "FAA Order 7130.3A, including all modifying FAA Memoranda, or its successor regulations, with the maximum allowed holding pattern airspeed from Table 1 and the inputs for FIX-to-NAVAID distance and holding altitude to identify the FAA template to apply to the holding pattern. The full size of the holding pattern for holding patterns in a location and at an altitude as published by the FAA or as assigned by FAA Air Traffic Control, shall be evaluated for obstacle clearance in accordance with FAA Order 7130.3A, including all modifying FAA Memoranda, paragraph 2-5, or its successor regulations. Left and right hand turns in holding patterns in FAA template tracing shall be accounted for in accordance with FAA Order 7130.3A, including all modifying FAA Memoranda, paragraphs 2-30.a and 2-30.b or its successor regulations.

The electronic holding pattern calculator will not be limited to solving the mathematical algorithms using arrays and tables alone. As technology advances and better digital electronic computing devices are developed, the holding pattern calculator will utilize that technology to calculate the holding pattern computations in real time without the use of tables and arrays by using the increased computing power of such devices. Some of these capabilities will include and not be limited to: real-time data inputs provided by the FMS instead of user prompted inputs, and automatically determining whether the hold needs to be 1.0 minute or 1.5 minutes inbound based on the current aircraft altitude.

Beginning at the end of the inbound leg (the fix) and triangulating once per second, the program generates an entire 360-degree turn using a selected bank angle and air speed. That curve is translated such that its end point is moved to the start of the inbound leg. A portion of the original curve will form the outbound turn and a portion of the translated curve will form the inbound turn. A search routine was used to locate the two points at which a straight line was tangent to both curves. The tangent point on the original curve is the start of the outbound leg. The tangent point on the translated curve is the end of the outbound leg. Because positions and bearings are known for all points on both curves, the program reports the bearing at the start of the outbound leg and calculates the bearing back to the NAVAID at the end of the outbound leg and that position is the start of the inbound turn.

When using triangulation to determine the path of a plane relative to the ground, the input values include bearing, altitude-corrected air speed, wind speed, and wind bearing. The spiral path generated includes the effect of wind. "Spiral path" is defined as a curved path with a continuously increasing radius of curvature. The FAA specifies maximum air speeds for holding patterns. Those vary with the type of aircraft and with altitude. The FAA also limits bank angles. Holding patterns that are smaller, are more likely to remain within protected space, with slower air speeds and greater bank angles. The program allows the pilot to select a bank angle and produces patterns for several air speeds equal to and less than the FAA maximum. The patterns are displayed graphically on the computer screen with the appropriate FAA envelope. The pilot can then visually select a pattern that remains within the protected space. If none do, he can rerun the program using a greater bank angle.

Using a known formula and the specified altitude, altitude-corrected air speeds are calculated from instrument-indicated air speeds. The altitude-corrected air speeds are used in the triangulation process along with other inputs to generate the path of the aircraft relative to the ground.

The computer program generates a graph for each of several air speeds. Each graph shows the path of the plane and the FAA envelope. The pilot can see visually where the path of the aircraft exits the envelope. He then selects a pattern that does not exit protected space and flies at that air speed.

In the present invention, the pilot uses a Flight Management System ("FMS") by inputting the required information to the computer and executing the program. He then selects one of the generated patterns to fly. The FMS is not a navigation system in itself. Rather, it is a system that automates the tasks of managing the onboard navigation systems. FMS's also perform other onboard management tasks.

FMS is an interface between flight crews and flight-deck systems. FMS can be thought of as a computer with a large

database of airport and NAVAID locations and associated data, aircraft performance data, airways, intersections, departure procedures ("DPs"), and standard terminal arrival routes ("STARs"). FMS also has the ability to accept and store numerous user-defined waypoints, flight routes consisting of departures, waypoints, arrivals, approaches, alternates, etc. FMS can quickly define a desired route from the aircraft's current position to any point in the world, perform flight plan computations, and display the total picture of the flight route to the crew.

FMS also has the capability of controlling (selecting) VOR, DME, and localizer ("LOC") NAVAIDs, and then receiving navigational data from them. Inertial Navigation System ("INS"), Long Range Navigation ("LORAN"), and GPS navigational data may also be accepted by the FMS computer. The FMS may act as the input/output device for the onboard navigation systems, so that it becomes the "go-between" for the crew and the navigation systems.

At startup, the crew programs the aircraft location, departure runway, DP (if applicable), waypoints defining the route, approach procedure, approach to be used, and routing to alternate. This may be entered manually, be in the form of a stored flight plan, or be a flight plan developed in another computer and transferred by disk or electronically to the FMS computer. The crew enters this basic information in the control/display unit (CDU). Once airborne, the FMS computer channels the appropriate NAVAIDs and takes radial/distance information, or channels two NAVAIDs, taking the more accurate distance information. FMS then indicates position, track, desired heading, groundspeed and position relative to desired track. Position information from the FMS updates the INS. In more sophisticated aircraft, the FMS provides inputs to the horizontal situtation indicator ("HSI"), radio-magnetic indicator ("RMI"), glass cockpit navigation displays, head-up display ("HUD"), autopilot, and autothrottle systems.

Once the required input information has been entered, within two to three minutes, depending on computer speed, the program calculates and displays the several patterns. An Automated Surface Observing System ("ASOS"), Automated Terminal Information Service ("ATIS"), Meteorological Terminal Aviation Routine weather reports ("METAR"), Terminal Aerodrome Forecast ("TAF"), or WINDS ALOFT may be used as data sources.

The inputs required for our computer program, whether entered by a flight management system or by the pilot, are latitude, longitude, and altitude of the NAVAID, the FAA number designation for the type of aircraft, the altitude of the aircraft during holding, the NAVAID to FIX distance and bearing, the direction of the outbound turn (right or left), the wind speed and bearing, the hold bearing, and the bank angle during turns. Micro Air Data Computers ("MADCs") provide to the FMS Barometric Altitude, Pressure Altitude, Indicated Airspeed, True Airspeed, Mach number, Vertical Airspeed, Maximum Operating Airspeed, Static and Total Air Temperature. (The true air speed computation is derived from calibrated airspeed, temperature, and pressure altitude). The MSU (Magnetic Sensor Unit) detects the horizontal component of the earth's magnetic field and transmits it to the Attitude and Heading Reference Unit ("AHRU") for use as long term heading reference. In MSU calibration mode, the AHRU determines the MSU calibration coefficients used for compensation of single and dual cycle MSU errors. The MSU calibration algorithm is able to compensate single and dual cycle errors in sum up to 12 degrees. The AHRS is a strap down inertial measurement system using fiber optic rate gyros and micromechanical accelerometers that are "strapped down" to the principle aircraft axes. A digital computer mathematically integrates the rate data to obtain heading, pitch, and roll.

The FAA specifies a one-minute inbound leg for altitudes less than or equal to 14,000 feet. Above 14,000 feet, the inbound leg is 1.5 minutes. The time elapsed during the outbound leg is calculated from the ground speed and the distance between the starting point of the leg and its end.

The steps in using the present invention to calculate a left or right hand aeronautical holding pattern can be summarized as follows:

(a) determining wind speed and direction;

(b) choosing a direction of a holding pattern from the group comprising left-hand and right-hand;

(c) selecting a start point and an end point of an inbound leg of the holding pattern;

(d) generating, with an electronic processor and by solving differential equations (or by repeated triangulation), a spiral path of an aircraft given the wind speed and direction determined in step (a) making a turn in the direction chosen in step (b);

(e) copying and translating the spiral path, with the electronic processor, so that for a first copy its starting point is the end point of the inbound leg selected in step (c), and for a second copy its ending point is the start point of the inbound leg selected in step (c);

(f) running a search routine, with the electronic processor, to locate positions on the first and second copy of the spiral path that have, as close as possible, the same bearing; and

(g) making the positions located in step (f) the start and end points of an outbound leg of the holding pattern;

(h) notifying a pilot, using the electronic processor, of a maximum allowed holding pattern airspeed for an aircraft;

(i) inputting a bank angle selected by the pilot into the electronic processor;

(j) generating and displaying, using the electronic processor, holding patterns for the maximum allowed airspeed and at least two lesser airspeeds;

(k) displaying boundaries of a protected airspace within which the aircraft must fly with the holding patterns of step (j), enabling the pilot to see if the holding patterns are within the protected airspace;

(l) if none of the holding patterns of step (j) are within the protected airspace, enabling the pilot to input a greater bank angle into the electronic processor, and generating and displaying new holding patterns using the electronic processor; and

(m) using global positioning data to display the position of the aircraft in the display of the holding patterns and boundaries of the protected airspace.

If there is no wind, the spiral path becomes circular. All of these steps will require the use of a computer or other electronic processor, which may be a stand alone device, or integrated into the system of an aircraft. Without generating projections from both the first and second copy of the spiral path simultaneously, one will frequently identify incorrect points.

If the spiral path generated in step (d) is generated by solving differential equations, it is preferably constructed from solutions of the following differential equations, where the fix is the ending point of the inbound leg, and is set at the origin (0, 0), and the x- and y-positions (with x being the east-west dimension and y being the north-south dimension), with east and north being the postive directions) of the aircraft at time t (in seconds) are:

$$x = as\{\sin[abo+(dps)t]/dps\}+ws[\cos(wb)]t$$

$$y = -as\{\cos[abo+(dps)t)]/dps\}+ws[\sin(wb)]t$$

wherein:

dps=rate of change in the bearing in radians per second;

as=air speed in meters per second;

ws=wind speed in meters per second;

wb=standard position angle representation of the wind bearing in radians; and

abo=inbound bearing in radians represented as an angle in standard position.

An important advantage of the present invention relates to variable bank and airspeed. Bank is usually constant and maintained with the flight director and autopilot. Allowing the pilot to alter the bank and then choose an airspeed appropriate for the hold is a unique feature, especially when combined with the visual presentation. Incoming GPS data may be stored in a file that is repetitively read into the computer program, which then displays the position of the aircraft on the same graph as the holding pattern.

The following are examples of using the present invention to calculate right hand (clockwise) holding patterns, showing prompts and output displayed by the computer, and data input by the user in bold: (Everything is displayed, except what is enclosed in parentheses, but including what is enclosed in brackets and single digits enclosed in parentheses.)

After each input, type a semicolon and then press Enter. Input NAVAID latitude in brackets, [N or S,degrees,minutes,seconds] Type semicolon. Press ENTER. [N,31,38,16];

Input NAVAID longitude in brackets, [E or W,degrees,minutes,seconds] Type semicolon. Press ENTER. [W,97,4,45];

Input NAVAID elevation in feet. Type semicolon. Press ENTER. 516;

Civil Aircraft (Classified by Maximum Holding Altitude ("MHA"))

(1) MHA through 6,000 ft.

(2) Above 6,000 ft through 14,000 ft

(3) Above 14,000 ft

Military Aircraft

(4) All except aircraft listed below

(5) T-38, F-15, and F-16

(6) USAF F-4 Aircraft

(7) B-1, F-111, and F-5

(8) T-37

Input the integer of plane type followed by semicolon. Then press ENTER. 3;

("Plane type" for civil aircraft is used loosely to refer to altitude range.)

MAXIMUM AIRSPEED=265 KIAS

Input altitude in feet (No commas) followed by semicolon. Then press ENTER. 15000;

Input NAVAID to FIX distance in NM followed by semicolon. Then press ENTER. 12;

Input NAVAID to FIX bearing in degrees followed by semicolon. Then press ENTER. 325;

Input holding bearing in degrees. 45;

Input 1 for Right Turn, 2 for Left Turn, 3 for FIG. **8**. Type semicolon. Then press ENTER. 1;

Input wind speed in knots. 30;

Input direction wind is blowing FROM, in degrees. 125;

Input bank angle in degrees. 20;

LATITUDE OF FIX=N 31 degrees, 48.08 minutes.

LONGITUDE OF FIX=W 97 degrees, 12.84 minutes.

FIX to NAVAID SLANT DME=12.23 NM

Holding Bearing=045 degrees.

Inbound Bearing=225 degrees.

Altitude=15000 feet.

Wind Blowing From=125 degrees.

Wind Blowing Toward=305 degrees.

Wind Speed=30 knots.

PATTERN 1 (**40** shown in FIG. **4**):

Indicated Inbound Air Speed=186 knots.

Altitude-Corrected Inbound Air Speed=241 knots.

Inbound ground speed=245 knots.

WIND CORRECTED INBOUND BEARING=218 degrees.

Turn "RIGHT" (at FIX **42**) with bank angle=20 degrees [1.65 degrees/second] (the outbound turn **44**) to outbound wind corrected bearing of 67 degrees (at post **46**, the start of outbound leg **48**).

Fly on that outbound heading for 105 seconds until the bearing back to NAVAID is 165 degrees (at post **50**, the end of the outbound leg).

Turn "RIGHT" with bank angle=20 degrees [1.65 degrees/second] (the inbound turn **52**) back to the start (at post **54**) of inbound leg **56**. (The end of the inbound leg is 42, the FIX where the holding pattern started and may be repeated.)

Latitude at end of outbound leg=N 31 degrees, 55.54 minutes.

Longitude at end of outbound leg=W 97 degrees, 10.24 minutes.

DME to NAVAID at end of outbound leg=18.07 NM.

(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15** (indicating the area within which the holding pattern is supposed to be contained).

Inbound leg=6.13 NM, Template **15** LM=9.60 NM, LI=7.70 NM.

(Directions are indicated by the larger circle **60** with compass points surrounding the FIX and the smaller circle **62** with compass points surrounding the NAVAID **64**. Cross lines **66** and nautical mile markers **67** indicate distance from the FIX. Line **68** indicates the direction of the inbound leg, which is toward the lower left. Line **70** indicates the distance and direction from the FIX to the NAVAID. Line **72** indicates the direction of the point **50** at which the outbound leg ends and the inbound turn begins to the NAVAID. Icon **74** indicates the wind corrected inbound heading. Icon **76** indicates the outbound wind corrected heading. Triangle **77** indicates the wind direction. The oval **58** is formed by two semicircles connected by straight line segments. One of the semicircles is centered on the FIX. LM is the distance between the fix and the center of the other semicircle. LI is the radius of both semicircles.)

PATTERN 2 (**78** shown in FIG. **5**):

Indicated Inbound Air Speed=225 knots.

Altitude-Corrected Inbound Air Speed=293 knots.

Inbound ground speed=297 knots.

WIND CORRECTED INBOUND BEARING=219 degrees.

Turn "RIGHT" (at FIX **42**) with bank angle=20 degrees [1.36 degrees/second] (the outbound turn **44**) to outbound wind corrected bearing of 67 degrees (at post **46**, the start of outbound leg **48**).

Fly on that outbound heading for 104 seconds until the bearing back to NAVAID is 166 degrees (at post **50**, the end of the outbound leg).

Turn "RIGHT" with bank angle=20 degrees [1.36 degrees/second] (the inbound turn **52**) back to start (at post **54**) of inbound leg (**56**). (The end of the inbound leg is 42, the FIX where the holding pattern started and may be repeated.)

Latitude at end of outbound leg=N 31 degrees, 58.09 minutes.

Longitude at end of outbound leg=W 97 degrees, 10.51 minutes.

DME to NAVAID at end of outbound leg=20.58 NM.

(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.

Inbound leg=7.42 NM, Template **15** LM=9.60 NM, LI=7.70 NM.

PATTERN 3 (**80** shown in FIG. **6**):

Indicated Inbound Air Speed=265 knots.

Altitude-Corrected Inbound Air Speed=344 knots.

Inbound ground speed=348 knots.
WIND CORRECTED INBOUND BEARING=220 degrees.
Turn "RIGHT" (at FIX **42**) with bank angle=20 degrees (1.15 degrees/second) (the outbound turn **44**) to outbound wind corrected bearing of 65 degrees (at post **46**, the start of outbound leg **48**).
Fly on that outbound heading for 103 seconds until the bearing back to NAVAID is 167 degrees (at post **50**, the end of the outbound leg).
Turn "RIGHT" with bank angle=20 degrees (1.15 degrees/second)(the inbound turn **52**) back to start (at post **54**) of inbound leg **56**. (The end of the inbound leg is 42, the FIX where the holding pattern started and may be repeated.)
Latitude at end of outbound leg=N 32 degrees, 0.96 minutes.
Longitude at end of outbound leg=W 97 degrees, 11.13 minutes.
DME to NAVAID at end of outbound leg=23.48 NM.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**. (Note that this holding pattern passes outside where FAA regulations say that it should be.)
Inbound leg=8.70 NM, Template **15** LM=9.60 NM, LI=7.70 NM.

(The following are examples of using the present invention to calculate left hand (counterclockwise) holding patterns, showing prompts and output displayed by the computer, and data input by the user in bold:)
After each input, type a semicolon and then press Enter.
Input NAVAID latitude in brackets,
[N or S, degrees, minutes, seconds] Type semicolon. Press ENTER. [N,31,38,16];
Input NAVAID longitude in brackets,
[E or W, degrees, minutes, seconds] Type semicolon. Press ENTER. [W,97,4,45];
Input NAVAID elevation in feet. Type semicolon. Press ENTER. 516;
Civil Aircraft
(1) MHA through 6,000 ft.
(2) Above 6,000 ft through 14,000 ft
(3) Above 14,000 ft
Military Aircraft
(4) All except aircraft listed below
(5) T-38, F-15, and F-16
(6) USAF F-4 Aircraft
(7) B-1, F-111, and F-5
(8) T-37
Input the integer of plane type followed by semicolon.
Then press ENTER. 3;
MAXIMUM AIRSPEED=265 KIAS
Input altitude in feet (No commas) followed by semicolon.
Then press ENTER. 15000;
Input NAVAID to FIX distance in NM followed by semicolon.
Then press ENTER. 12;
Input NAVAID to FIX bearing in degrees followed by semicolon.
Then press ENTER. 325;
Input holding bearing in degrees. 45;
Input 1 for Right Turn, 2 for Left Turn, 3 for FIG. **8**.
Type semicolon. Then press ENTER. 2;
Input wind speed in knots. 35;
Input direction wind is blowing FROM, in degrees. 125;
Input bank angle in degrees. 25;
LATITUDE OF FIX=N 31 degrees, 48.08 minutes.
LONGITUDE OF FIX=W 97 degrees, 12.84 minutes.
FIX to NAVAID SLANT DME=12.23 NM
Holding Bearing=045 degrees.
Inbound Bearing=225 degrees.
Altitude=15000 feet.
Wind Blowing From=125 degrees.
Wind Blowing Toward=305 degrees.
PATTERN 1 (**82** shown in FIG. **7**):
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=245 knots.
WIND CORRECTED INBOUND BEARING=217 degrees.
Turn "LEFT" (at FIX **42**) with bank angle=25 degrees [2.11 degrees/second] (the outbound turn **44**) to outbound wind corrected bearing of 69 degrees (at post **46**, the start of outbound leg **48**).
Fly on that outbound heading for 106 seconds until the bearing back to NAVAID is 182 degrees (at post **50**, the end of the outbound leg).
Turn "LEFT" with bank angle=25 degrees [2.11 degrees/second] (the inbound turn **52**) back to start (at post **54**) of inbound leg (**56**). (The end of the inbound leg is 42, the FIX where the holding pattern started and may be repeated.)
Latitude at end of outbound leg=N 31 degrees, 49.07 minutes.
Longitude at end of outbound leg=W 97 degrees, 4.31 minutes.
DME to NAVAID at end of outbound leg=11.09 NM.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.
Inbound leg=6.13 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
PATTERN 2 (**84** shown in FIG. **8**):
Indicated Inbound Air Speed=225 knots.
Altitude-Corrected Inbound Air Speed=293 knots.
Inbound ground speed=297 knots.
WIND CORRECTED INBOUND BEARING=218 degrees.
Turn "LEFT" (at FIX **42**) with bank angle=25 degrees [1.74 degrees/second] (the outbound turn **44**) to outbound wind corrected bearing of 67 degrees (at post **46**, the start of outbound leg **48**).
Fly on that outbound heading for 105 seconds until the bearing back to NAVAID is 194 degrees (at post **50**, the end of the outbound leg).
Turn "LEFT" with bank angle=25 degrees [1.74 degrees/second] (the inbound turn **52**) (back to start (at post **54**) of inbound leg **56**).
Latitude at end of outbound leg=N 31 degrees, 48.58 minutes.
Longitude at end of outbound leg=W 97 degrees, 1.73 minutes.
DME to NAVAID at end of outbound leg=10.92 NM.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.
Inbound leg=7.42 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
PATTERN 3 (**86** shown in FIG. **9**):
Indicated Inbound Air Speed=265 knots.
Altitude-Corrected Inbound Air Speed=344 knots.
Inbound ground speed=349 knots.
WIND CORRECTED INBOUND BEARING=219 degrees.
Turn "LEFT" with bank angle=25 degrees [1.48 degrees/second] (the outbound turn **44**) to outbound wind corrected bearing of 65 degrees (at post **46**, the start of outbound leg **48**).
Fly on that outbound heading for 104 seconds until the bearing back to NAVAID is 207 degrees (at post **50**, the end of the outbound leg).
Turn "LEFT" with bank angle=25 degrees [1.48 degrees/second] (the inbound turn **52**) (back to start (at post **54**) of inbound leg **56**).

Latitude at end of outbound leg=N 31 degrees, 47.84 minutes.
Longitude at end of outbound leg=W 96 degrees, 58.93 minutes.
DME to NAVAID at end of outbound leg=11.06 NM.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**. (Note that this holding pattern passes outside where FAA regulations say that it should be.)
Inbound leg=8.73 NM, Template **15** LM=9.60 NM, LI=7.70 NM.

Figure eight holding patterns are a unique alternative to regular holding patterns, that may be used when the winds are very high and are perpendicular to the inbound holding course. The figure eight patterns have two turns into the wind direction, which minimizes the chance of being blown outside of the protected holding airspace. Optimum conditions for these patterns are high velocity winds perpendicular to the inbound course, or not more than +30 degrees or −30 degrees from perpendicular in relation to the inbound course. For example, if the inbound course is on the 360 degree radial, heading 180 degrees (south), and the wind is from 90 degrees (east) at 80 knots or greater. A figure eight pattern would work just as well for that inbound course, heading and wind speed, with wind having a bearing up to 30 degrees less than 90 degrees (e.g., 80, 70 or 60 degrees) or up to 30 degrees more (e.g., 100, 110 or 120 degrees). Except in this type of scenario, a regular holding pattern should be used.

Computer-generated simulated figure eight flight paths indicate holding patterns will occupy less air space as the acute angle between wind direction and the hold bearing increases. Figure eight holding patterns cannot be successfully completed when moderate winds flow close to parallel to the hold bearing. Patterns were generated for the condition where the aircraft turns into wind at both ends of the inbound leg. Patterns differ slightly when the aircraft has a headwind rather than a tailwind on entering the inbound leg. Figure eight holding patterns can be very compact under high wind conditions, provided that the wind direction is nearly perpendicular to the hold bearing. In light winds, Figure eight patterns can be successfully completed only when the wind direction is not close to perpendicular to the inbound leg. Figure eight holding patterns must be more compact than elliptical holding patterns to remain within the airspace required by FAA Order 7130.3A or its successor regulations.

The steps in using the present invention to calculate a figure eight aeronautical holding pattern can be summarized as follows:

(a) determining wind speed and direction;

(b) selecting a start point and an end point of an inbound leg of the holding pattern;

(c) generating, with an electronic processor and by solving differential equations (or by repeated triangulation), a first spiral path of an aircraft given the wind speed and direction determined in step (a) and making a turn into the wind;

(d) copying and translating the first spiral path, with the electronic processor, so that for a first copy its starting point is the end point of the inbound leg selected in step (b), and for a second copy its ending point is the end point of the inbound leg selected in step (b);

(e) generating, with an electronic processor and by solving differential equations (or by repeated triangulation), a second spiral path of an aircraft given the wind speed and direction determined in step (a) and making a turn in the opposite direction from the turn in step (c);

(f) copying and translating the second spiral path, with the electronic processor, so that for a third copy its starting point is the start point of the inbound leg selected in step (b), and for a fourth copy its ending point is the start point of the inbound leg selected in step (b);

(g) running a search routine, with the electronic processor, to locate positions on the first and fourth copies that have, as close as possible, the same air bearing;

(h) making the positions located in step (g) the start and end points of a first straight line portion of the figure eight holding pattern;

(i) running a search routine, with the electronic processor, to locate positions on the second and third copies that have, as close as possible, the same bearing;

(j) making the positions located in step (i) the start and end points of a second straight line portion of the figure eight holding pattern;

(k) notifying a pilot, using the electronic processor, of a maximum allowed holding pattern airspeed for an aircraft;

(l) inputting a bank angle selected by the pilot into the electronic processor;

(m) generating and displaying, using the electronic processor, holding patterns for the maximum allowed airspeed and at least two lesser airspeeds;

(n) displaying boundaries of a protected airspace within which the aircraft must fly with the holding patterns of step (m), enabling the pilot to see if the holding patterns are within the protected airspace;

(o) if none of the holding patterns of step (m) are within the protected airspace, enabling the pilot to input a greater bank angle into the electronic processor, and generating and displaying new holding patterns using the electronic processor; and

(p) using global positioning data to display the position of the aircraft in the display of the holding patterns and boundaries of the protected airspace.

Again, if there is no wind, the spiral path becomes circular. As before, all of these steps will require the use of a computer or other electronic processor, which may be a stand alone device, or integrated into the system of an aircraft. Without generating projections from the copies of the spiral paths simultaneously, one will frequently identify incorrect points.

If the first and second spiral paths are generated by solving differential equations, it is preferable that they be constructed from solutions of the following differential equations, where the fix is the ending point of the inbound leg, and is set at the origin (0, 0), and the x- and y-positions of the aircraft at time t (in seconds) are:

$$x=\{[as\ \sin(abo+(dps)t)]/dps\}+ws\ \cos(wb)t$$

$$y=-\{[as\ \cos(abo+(dps)t)]/dps\}+ws\ \sin(wb)t$$

wherein:

dps=rate of change in the bearing in radians per second;

as=air speed in meters per second;

ws=wind speed in meters per second;

wb=standard position angle representation of the wind bearing in radians; and

abo=inbound bearing in radians represented as an angle in standard position.

The following are examples of using the present invention to calculate figure eight holding patterns, showing prompts and output displayed by the computer, and data input by the user in bold. (Everything is displayed, except what is enclosed in parentheses, but including what is enclosed in brackets and single digits enclosed in parentheses.) The following are common to all six patterns, except as indicated:
After each input, type a semicolon and then press Enter.
Input NAVAID latitude in brackets,

[N or S,degrees,minutes,seconds] Type semicolon.
Press ENTER. [N,31,38,16];
Input NAVAID longitude in brackets,
[E or W,degrees,minutes,seconds] Type semicolon. Press ENTER.
Input NAVAID elevation in feet. Type semicolon. Press ENTER. 516;
Civil Aircraft (Classified by MHA)
(1) MHA through 6,000 ft.
(2) Above 6,000 ft through 14,000 ft
(3) Above 14,000 ft
Military Aircraft
(4) All except aircraft listed below
(5) T-38, F-15, and F-16
(6) USAF F-4 Aircraft
(7) B-1, F-111, and F-5
(8) T-37
Input the integer of plane type followed by semicolon.
Then press ENTER. 3;
MAXIMUM AIRSPEED=265 KIAS
Input altitude in feet (No commas) followed by semicolon.
Then press ENTER. 15000;
Input NAVAID to FIX distance in NM followed by semicolon.
Then press ENTER. 12;
Input NAVAID to FIX bearing in degrees followed by semicolon.
Then press ENTER. 300;
Input holding bearing in degrees. 45;
Input 1 for Right Turn, 2 for Left Turn, 3 for FIG. **8** Right, 4 for Figure Eight Left. Type semicolon. Then press ENTER. 3;
Input wind speed in knots. 65;
Input direction wind is blowing FROM, in degrees. 325;
(Indicated by triangle **91**.)
Input bank angle in degrees. 20;
LATITUDE OF FIX=N 31 degrees, 44.25 minutes.
LONGITUDE OF FIX=W 97 degrees, 16.96 minutes.
FIX to NAVAID SLANT DME=12.23 NM
Xproduct=0.98
Holding Bearing=045 degrees.
Inbound Bearing=225 degrees.
Altitude=15,000 feet.
Wind Blowing From=325 degrees.
Wind Blowing Toward=145 degrees.
Wind Speed=65 knots.
PATTERN 1 (**88** shown in FIG. **10**—initial right turn when wind is from the right):
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=244 knots.
WIND CORRECTED INBOUND BEARING=240 degrees (as indicated by icon **90**.)
Enter the holding pattern at FIX **42**, and turn "RIGHT" until bearing is 60.0 degrees (at post **92**, the end of the outbound turn **94** and the beginning of the outbound leg **96**).
Level and fly that bearing until the bearing back to NAVAID is 144.8 degrees (at post **98**, the end of the outbound leg and the beginning of the inbound turn **100**).
(At post **98**) Turn "LEFT", (passing through tangent point **108**,) until bearing is 200.0 degrees (at post **102**, the beginning of the inbound leg **104**).
(Level and fly that bearing until the) Bearing back to NAVAID is 127.5 degrees (at post **105**, the end of the inbound leg and the beginning of the outbound turn **94**).
(Begin "RIGHT" turn (on outbound turn **94**) and repeat circuit.)
(Note that the outbound turn begins before the FIX.)
Start of Inbound leg to NAVAID Slant DME=12.21 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.57 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 11.90 minutes.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.
Inbound leg=6.10 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
(Line **106** indicates the inbound bearing, and passes through the FIX **42** and a tangent point **108** on the inbound turn **100**.)
PATTERN 2 (**110** shown in FIG. **11**—initial right turn when wind is from the right):
Input direction wind is blowing FROM, in degrees. 305;
(Indicated by triangle **91**.)
Wind Blowing From=305 degrees.
Wind Blowing Toward=125 degrees.
Wind Speed=65 knots.
Indicated Inbound, Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=221 knots.
WIND CORRECTED INBOUND BEARING=240 degrees.
Enter the holding pattern at FIX **42**, and turn "RIGHT" until bearing is 78.0 degrees (at post **92**, the end of the outbound turn **94** and the beginning of the outbound leg **96**).
(Level and fly that bearing until the) Bearing back to NAVAID is 137.8 degrees (at post **98**, the end of the outbound leg and the beginning of the inbound turn **100**).
(At post **98**) Turn "LEFT", (passing through tangent point **108**,) until bearing is 205.0 degrees (at post **102**, the beginning of the inbound leg **104**).
(Level and fly that bearing until the) Bearing back to NAVAID is 126.0 degrees (at post **105**, the end of the inbound leg and the beginning of the outbound turn **94**).
Begin "RIGHT" turn (on outbound turn **94**) and repeat circuit.
Start of Inbound leg to NAVAID Slant DME=12.08 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.16 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 12.37 minutes.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.
Inbound leg=5.52 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
PATTERN 3 (shown as **112** in FIG. **12**—initial right turn when wind is from the left):
Input direction wind is blowing FROM, in degrees. 125;
(Indicated by triangle **91**.)
Xproduct=−0.98
Wind Blowing From=125 degrees.
Wind Blowing Toward=305 degrees.
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=244 knots.
WIND CORRECTED INBOUND BEARING=210 degrees.
Enter the holding pattern at tangent point **108** (on inbound turn **100**) and turn RIGHT until bearing is 250.0 degrees (at post **98**, the end of the inbound turn and the beginning of the inbound leg **96**).
Level and fly that bearing until the bearing back to NAVAID is 129.6 degrees (at post **92**, the end of the inbound leg and the beginning of the outbound turn **94**).
(At that point) Turn LEFT (passing through the FIX **42**) until bearing is 30.0 degrees (at post **105**, the end of the outbound turn and the beginning of the outbound leg **104**). (Level and

fly that bearing (on inbound turn **100**) until the) Bearing back to NAVAID is 144.3 degrees (at post **102**).
(Begin RIGHT turn (on inbound turn **100**) and repeat circuit.)
Start of Inbound leg to NAVAID Slant DME=12.21 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.57 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 11.90 minutes.
(Area enclosed in blue is a) Subset of FAA Basic Template **15**.
Inbound leg=6.10 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
PATTERN 4 (113 shown in FIG. **13**—initial left turn when wind is from the right):
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=244 knots.
WIND CORRECTED INBOUND BEARING=240 degrees.
Enter the holding pattern at tangent point **108** (on inbound turn **100**) turn LEFT until bearing is 200.0 degrees (at post **98**, the end of the inbound turn and the start of the inbound leg **104**).
Level and fly that bearing until the bearing back to NAVAID is 126.9 degrees (at post **92**, the end of the inbound leg and the start of outbound turn **94**).
(At post **92**) Turn RIGHT (passing through the FIX **42**) until bearing is 60.0 degrees (at post **105**, the end of the outbound turn and the start of outbound leg **96**).
(Level and fly that bearing until the) Bearing back to NAVAID is 149.5 degrees (at post **102**).
(Begin LEFT turn (on inbound turn **100**) and repeat circuit.)
Start of Inbound leg to NAVAID Slant DME=12.21 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.57 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 11.90 minutes.
(Area enclosed in oval **58** is a) Subset of FAA Basic Template **15**.
Inbound leg=6.10 NM, Template **15** LM=9.60 NM, LI=7.70 NM
PATTERN 5 (**115** shown in FIG. **14**—initial left turn when wind is from the right):
Input direction wind is blowing FROM, in degrees. 305;
(Indicated by triangle **91**.)
Wind Blowing From=305 degrees.
Wind Blowing Toward=125 degrees.
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=221 knots.
WIND CORRECTED INBOUND BEARING=240 degrees.
(Enter the holding pattern at tangent point **108** on inbound turn **100**.) Turn LEFT until bearing is 205.0 degrees (at post **98**, the end of the inbound turn and the start of inbound leg **104**). (Level and fly that bearing until the) Bearing back to NAVAID is 121.5 degrees (at post **92**, the end of the inbound leg and the start of outbound turn **94**).
(At that point) Turn RIGHT (passing through the FIX **42**) until bearing is 78.0 degrees (at post **105**, the end of the outbound turn and the start of the outbound leg **96**).
(Level and fly that bearing until the) Bearing back to NAVAID is 136.9 degrees (at post **102**).
(Begin) LEFT turn (on inbound turn **100** and repeat circuit).
Start of Inbound leg to NAVAID Slant DME=12.08 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.16 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 12.37 minutes.
(Area enclosed in blue is a) Subset of FAA Basic Template **15**.
Inbound leg=5.52 NM, Template **15** LM=9.60 NM, LI=7.70 NM.
PATTERN 6. (**117** shown in FIG. **15**—initial left turn when wind is from the left):
Input direction wind is blowing FROM, in degrees. 145;
(Indicated by triangle **91**.)
Xproduct=−0.98
Wind Blowing From=145 degrees.
Wind Blowing Toward=325 degrees.
Indicated Inbound Air Speed=186 knots.
Altitude-Corrected Inbound Air Speed=241 knots.
Inbound ground speed=221 knots.
WIND CORRECTED INBOUND BEARING=210 degrees.
Enter the holding pattern at FIX **42** (on outbound turn **94**) and turn "LEFT" until bearing is 12.0 degrees (at post **92**, the end of outbound turn **94** and the start of outbound leg **104**).
(Level and fly that bearing until the) Bearing back to NAVAID is 138.5 degrees (at post **98**, the end of the outbound leg and the start of inbound turn **100**).
(At post **98**) "RIGHT" (passing through tangent point **108**) until bearing is 245.0 degrees (at post **102**, the end of the inbound turn and the start of inbound leg **96**).
(Level and fly that bearing until the) Bearing back to NAVAID is 125.3 degrees (at post **105**, the end of the inbound leg and the start of outbound turn **94**).
(Begin "LEFT" turn (on outbound turn **94**) and repeat circuit.)
Start of Inbound leg to NAVAID Slant DME=12.08 NM.
LATITUDE OF START OF INBOUND LEG=N 31 degrees, 48.16 minutes.
LONGITUDE OF START OF INBOUND LEG=W 97 degrees, 12.37 minutes.
(Area enclosed in blue is a) Subset of FAA Basic Template **15**.
Inbound leg=5.52 NM, Template **15** LM=9.60 NM, LI=7.70 NM.

FIGS. **16-23** are flowcharts showing how the invention may be implemented using a computer program. They are for illustration only. Other types of computer programs may be used to implement the invention.

In FIG. **16**, the program first specifies certain variables as being local to the program **114**, such as local coordinates, hold bearing, air speed, altitude, wind speed, etc. The code then collects input values **116**, such as NAVAID latitude, longitude, elevation, aircraft type, and maximum speed. Maximum air speed is then printed or otherwise outputted **118**. The code again collects input values **120**, such as altitude, and NAVAID to FIX distance and bearing. Earth radius is calculated **122**. The latitude of the fix is calculated **124**. The longitude of the fix is calculated **126**. The slant distance from the fix to the NAVAID is then calculated **128**.

In FIG. **17**, the program then collects inputs of the hold bearing, turn direction, wind speed, and wind bearing **130**. The FAA envelope is selected using the FIX to NAVAID distance, altitude, and maximum air speed **132**. FAA distance values for various envelopes are listed **134**. The bank angle is inputted **136**. The latitude and longitude of the FIX and FIX to NAVAID slant distance are printed or otherwise outputted **138**. The bearings may be converted to standard position angles **140**. A plot of an icon in the form of an arrow indicating direction is created **142**. The format of bearings for future output is adjusted **144**.

In FIG. **18**, wind bearing and wind speed are printed or otherwise outputted **146**. The program checks to see if wind speed is too great **148**. Plots are created for future output **150**. Loops for three air speeds are initiated **152**. Output and altitude-corrected air speeds are indicated **154**. Rate of turn from bank angle is calculated **156**. Variables such as degrees per

second and wind bearing are reset **158**. Calculate the bearing and ground speed for the inbound leg are calculated **160**.

In FIG. **19**, if the holding pattern is a figure eight **162**, calculate the bearing and ground speed for the second spiral needed for a figure eight holding pattern **164**. Then, regardless of the type of holding pattern, calculate bearing and ground speed for the inbound leg **166**. Adjust the format of the bearings for future output **168**. Output inbound bearing **170**. Create plots to draw airplanes on graph **172**. Create text plots to display bearing values on graph **174**, and set the FIX at the origin (0, 0) **176**.

In FIG. **20**, if the altitude is greater than 14,000 feet **178**, set the time of the inbound leg to 1.5 minutes **180**, else set the time of the inbound leg to 1.0 minutes **182**. Calculate the x- and y-coordinates of the start of the inbound leg **184**. Calculate the length of the inbound leg **186**. The program then draws the FAA envelope and the LM line (**68** in FIG. **4-9** or **106** in FIGS. **10-12**) **188**. If the holding pattern is for a left turn **190**, set rate of turn **192**. If the holding pattern is a figure eight **194**, the computer decides which way to turn to turn into the wind **196**. Regardless of the type of holding pattern, next it generates a first 360-degree spiral **198**. If and only if the holding pattern is a figure eight **200**, it generates a second 360-degree spiral **202**. Regardless of the type of holding pattern, it next calculate the x- and y-coordinates of the NAVAID **204**. It then sets a large number **206**, that is the maximum number of degrees that the wind direction can vary for the holding pattern.

In FIG. **21**, if the holding pattern is not a figure eight **208** (i.e., is a left or right turn), set the search region to find start and stop of the outbound leg **210**, and proceed to F in FIG. **22**. If the holding pattern is a figure eight, set search regions for locating start and stop locations for two straight line legs **212**, perform search routines to locate start and stop locations for straight line portions of figure eight pattern and generate coordinates along the figure eight path **214**, tell the pilot which way to turn, when to fly straight, and when to start and stop second turn to complete the figure eight **216**, plot the figure eight **218**, draw circles at the ends of the straight line portions **220**, and proceed to G in FIG. **22**.

In FIG. **22**, for right or left turns, the program searches to find the start and stop of the outbound leg **222**, and generate the coordinates of points along the flight path **224**. For any kind of holding pattern, the program then calculates the bearing back to the NAVAID at end of outbound leg **226**. Then it calculates the latitude and longitude of the end of the outbound leg **228**. It generates the plots to draw the FAA envelope **230**. It calculates the slant DME from the end of the outbound leg to the NAVAID **232**. It generates plots, marking 10-degree intervals **234** on a circle, and marking 90-degree intervals **236** (with larger marks) on the circle. (It may modify the format of bearings for output.) Then, it writes words on a graph or other display **238**.

In FIG. **23**, if FIX and NAVAID are not the same location **240**, print the bearing **242**. In either case, draw airplane images **244**, and generate output text and plots **246**. If the holding pattern is not a figure eight **248**, display the graph with all plots and text plots **250** for a left or right hand holding pattern. If the holding pattern is a figure eight, display the graph with all plots and text plots **252** for a figure eight holding pattern.

It is to be understood that the present invention is not limited to the embodiments described above, but encompasses any and all embodiments within the scope of the following claims.

We claim:

1. A method of calculating a Federal Aviation Administration (FAA) published or FAA Air Traffic Control assigned aeronautical holding pattern, comprising the steps of:

(a) determining wind speed and direction;

(b) choosing a direction of a holding pattern from the group comprising left-hand and right-hand;

(c) selecting a start point and an end point of an inbound leg of the holding pattern;

(d) generating, with an electronic processor and by solving differential equations, a spiral path of an aircraft given the wind speed and direction determined in step (a) making a turn in the direction chosen in step (b);

(e) copying and translating the spiral path, with the electronic processor, so that for a first copy its starting point is the end point of the inbound leg selected in step (c), and for a second copy its ending point is the start point of the inbound leg selected in step (c);

(f) running a search routine, with the electronic processor, to locate positions on the first and second copy of the spiral path that have, as close as possible, the same bearing;

(g) making the positions located in step (f) the start and end points of an outbound leg of the holding pattern; and

(h) flying an aircraft in the holding pattern;

wherein, "spiral path" is defined as a curved path with a continuously increasing radius of curvature.

2. The method of calculating an aeronautical holding pattern according to claim **1**, comprising the further steps of:

(i) notifying a pilot, using the electronic processor, of a maximum allowed holding pattern airspeed for an aircraft;

(j) inputting a bank angle selected by the pilot into the electronic processor;

(k) generating and displaying, using the electronic processor, holding patterns for the maximum allowed airspeed and at least two lesser airspeeds;

(l) displaying boundaries of a protected airspace within which the aircraft must fly with the holding patterns of step (k), enabling the pilot to see if the holding patterns are within the protected airspace; and

(m) if none of the holding patterns of step (k) are within the protected airspace, enabling the pilot to input a greater bank angle into the electronic processor, and generating and displaying new holding patterns using the electronic processor.

3. The method of calculating an aeronautical holding pattern according to claim **2**, comprising the further step of:

using global positioning data to display the position of the aircraft in the display of the holding patterns and boundaries of the protected airspace.

4. The method of calculating an aeronautical holding pattern according to claim **1**, wherein:

the spiral path generated in step (d) is constructed from solutions of the following differential equations, where the fix is the ending point of the inbound leg, and is set at the origin (0, 0), and the x- and y-positions of the aircraft at time t (in seconds) are:

$$x=as\{\sin[abo+(dps)t]/dps\}+ws[\cos(wb)]t$$

$$y=-as\{\cos[abo+(dps)t)]/dps\}+ws[\sin(wb)]t$$

wherein:

dps=rate of change in the air bearing in radians per second;

as=air speed in meters per second;

ws=wind speed in meters per second;

wb=standard position angle representation of the wind bearing in radians; and

abo=inbound air bearing in radians represented as an angle in standard position.

5. The method of calculating an aeronautical holding pattern according to claim **1**, wherein when there is no wind, the spiral path becomes circular.

6. The method of calculating an aeronautical holding pattern according to claim **1**, wherein the electronic processor is in a stand alone device.

7. The method of calculating an aeronautical holding pattern according to claim **1**, wherein the electronic processor is integrated into a system of an aircraft.

8. A method of calculating a Federal Aviation Administration (FAA) published or FAA Air Traffic Control assigned aeronautical holding pattern, comprising the steps of:

(a) determining wind speed and direction;

(b) choosing a direction of a holding pattern from the group comprising left-hand and right-hand;

(c) selecting a start point and an end point of an inbound leg of the holding pattern;

(d) generating, with an electronic processor and by repeated triangulation, a spiral path of an aircraft given the wind speed and direction determined in step (a) making a turn in the direction chosen in step (b);

(e) copying and translating the spiral path, with the electronic processor, so that for a first copy its starting point is the end point of the inbound leg selected in step (c), and for a second copy its ending point is the start point of the inbound leg selected in step (c);

(f) running a search routine, with the electronic processor, to locate positions on the first and second copy of the spiral path that have, as close as possible, the same bearing;

(g) making the positions located in step (f) the start and end points of an outbound leg of the holding pattern; and

(h) flying an aircraft in the holding pattern;

wherein, "spiral path" is defined as a curved path with a continuously increasing radius of curvature.

9. The method of calculating an aeronautical holding pattern according to claim **8**, comprising the further steps of:

(i) notifying a pilot, using the electronic processor, of a maximum allowed holding pattern airspeed for an aircraft;

(j) inputting a bank angle selected by the pilot into the electronic processor;

(k) generating and displaying, using the electronic processor, holding patterns for the maximum allowed airspeed and at least two lesser airspeeds;

(l) displaying boundaries of a protected airspace within which the aircraft must fly with the holding patterns of step (k), enabling the pilot to see if the holding patterns are within the protected airspace; and

(m) if none of the holding patterns of step (k) are within the protected airspace, enabling the pilot to input a greater bank angle into the electronic processor, and generating and displaying new holding patterns using the electronic processor.

10. The method of calculating an aeronautical holding pattern according to claim **9**, comprising the further step of:

using global positioning data to display the position of the aircraft in the display of the holding patterns and boundaries of the protected airspace.

11. The method of calculating an aeronautical holding pattern according to claim **8**, wherein when there is no wind, the spiral path becomes circular.

12. The method of calculating an aeronautical holding pattern according to claim **8**, wherein the electronic processor is in a stand alone device.

13. The method of calculating an aeronautical holding pattern according to claim **8**, wherein the electronic processor is integrated into a system of an aircraft.

14. A method of calculating a figure eight aeronautical holding pattern, in a location and at an altitude as published by the FAA or as assigned by FAA Air Traffic Control, comprising the steps of:

(a) determining wind speed and direction;

(b) selecting a start point and an end point of an inbound leg of the holding pattern;

(c) generating, with an electronic processor and by using methods selected from the group comprising solving differential equations and repeated triangulation, a first spiral path of an aircraft given the wind speed and direction determined in step (a) and making a turn into the wind;

(d) copying and translating the first spiral path, with the electronic processor, so that for a first copy its starting point is the end point of the inbound leg selected in step (b), and for a second copy its ending point is the end point of the inbound leg selected in step (b);

(e) generating, with an electronic processor and by using methods selected from the group comprising solving differential equations and repeated triangulation, a second spiral path of an aircraft given the wind speed and direction determined in step (a) and making a turn in the opposite direction from the turn in step (c);

(f) copying and translating the second spiral path, with the electronic processor, so that for a third copy its starting point is the start point of the inbound leg selected in step (b), and for a fourth copy its ending point is the start point of the inbound leg selected in step (b);

(g) running a search routine, with the electronic processor, to locate positions on the first and fourth copies that have, as close as possible, the same bearing;

(h) making the positions located in step (g) the start and end points of a first straight line portion of the figure eight holding pattern;

(i) running a search routine, with the electronic processor, to locate positions on the second and third copies that have, as close as possible, the same bearing;

(j) making the positions located in step (i) the start and end points of a second straight line portion of the figure eight holding pattern; and

(k) flying an aircraft in the holding pattern;

wherein, "spiral path" is defined as a curved path with a continuously increasing radius of curvature.

15. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, comprising the further steps of:

(l) notifying a pilot, using the electronic processor, of a maximum allowed holding pattern airspeed for an aircraft;

(m) inputting a bank angle selected by the pilot into the electronic processor;

(n) generating and displaying, using the electronic processor, holding patterns for the maximum allowed airspeed and at least two lesser airspeeds;

(o) displaying boundaries of a protected airspace within which the aircraft must fly with the holding patterns of step (n), enabling the pilot to see if the holding patterns are within the protected airspace; and

(p) if none of the holding patterns of step (n) are within the protected airspace, enabling the pilot to input a greater

bank angle into the electronic processor, and generating and displaying new holding patterns using the electronic processor.

16. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, comprising the further step of:

using global positioning data to display the position of the aircraft in the display of the holding patterns and boundaries of the protected airspace.

17. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, wherein:

the first and second spiral paths are constructed from solutions of the following differential equations, where the fix is the ending point of the inbound leg, and is set at the origin (0, 0), and the x- and y-positions of the aircraft at time t (in seconds) are:

$$x=\{[as\ \sin(abo+(dps)t)]/dps\}+ws\ \cos(wb)t$$

$$y=-\{[as\ \cos(abo+(dps)t)]/dps\}+ws\ \sin(wb)t$$

wherein:

dps=rate of change in the air bearing in radians per second;

as=air speed in meters per second;

ws=wind speed in meters per second;

wb=standard position angle representation of the wind bearing in radians; and

abo=inbound air bearing in radians represented as an angle in standard position.

18. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, wherein when there is no wind, the spiral paths become circular.

19. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, wherein the electronic processor is in a stand alone device.

20. The method of calculating a figure eight aeronautical holding pattern according to claim **14**, wherein the electronic processor is integrated into a system of an aircraft.

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